Department of Environment, Health and Natural Resources Division of Environmental Health On-Site Wastewater Section

Sheet: Property ID: Lot #:

Lot #: File #: Code:

5502111-0087

## SOIL/SITE EVALUATION for ON-SITE WASTEWATER SYSTEM

WALKER GROWE Owner: Applicant: TOUR HOMES LIC Address: 171 WALVER (2W) Date Evaluated: (2/08/202)

Proposed Facility: 3M SS Design Flow (.1949):

Location of Site: Property Recorded: Property Size: Public Individual ☐ Well ☐ Spring Other Water Supply: Pit Industrial Process Evaluation Method: Auger Boring ☐ Cut Sewage Type of Wastewater: ☐ Mixed

| P<br>R<br>O<br>F<br>I<br>L<br>E | .1940<br>Landscape<br>Position/<br>Slope % | Horizon<br>Depth<br>(ln.) | SOIL MORPHOLOGY<br>.1941       |                                    | OTHER<br>PROFILE FACTORS           |                              |                         |                         |                            |
|---------------------------------|--|---------------------------|--------------------------------|------------------------------------|------------------------------------|------------------------------|-------------------------|-------------------------|----------------------------|
|                                 |  |                           | .1941<br>Structure/<br>Texture | .1941<br>Consistence<br>Mineralogy | .1942<br>Soil<br>Wetness/<br>Color | .1943<br>Soil<br>Depth (IN.) | .1956<br>Sapro<br>Class | .1944<br>Restr<br>Horiz | Profile<br>Class<br>& LTAR |
| 1,2                             | L 3%                                       | 0-14                      | or is                          | M NSNP                             |                                    |                              |                         |                         | PS                         |
|                                 |  | 14-42                     | on ou                          | FR SP                              | 7.5727, C46"                       | 42                           |                         |                         | 6.35                       |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
| 3                               | L 350                                      | 0-14                      | Ca is                          | VA NONP                            |                                    |                              |                         |                         | PS                         |
|                                 |  | 14-38                     | me sic                         | F1 3P                              | 7.5427,036"                        | 3%                           |                         |                         | G.35                       |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                 |  |                           |                                |                                    |                                    |                              |                         |                         |                            |

| Description                       | Initial | Repair System | Other Factors (.1946):       |                      |
|-----------------------------------|---------|---------------|------------------------------|----------------------|
| 7000000000000 <b>*</b> 0 70000000 | System  |               | Site Classification (.1948): | PROSIONALLY SUITABLE |
| Available Space (.1945)           |         |               | Evaluated By:                |                      |
| System Type(s)                    | 25% TO  | 75% TES       | Others Present:              | ANDREW WARDN, NEHS   |
| Site LTAR                         | 6.35    | 0.35          |                              |                      |

COMMENTS: \_\_\_\_

| LANDSCAPE POSITIONS                                       | <u>GROUP</u> | <u>TEXTURES</u>   | . <u>1955 LTAR</u> | CONSISTENCE MOIST                              | WET  |  |
|---|--------------|---|--------------------|--|--|--|
| R-RIDGE<br>S-SHOULDER SLOPE<br>L-LINEAR SLOPE             | Ĭ            | S-SAND<br>LS-LOAMY SAND   | 1.2 - 0.8          | VFR-VERY FRIABLE<br>FR-FRIABLE                 | NS-NON-STICKY<br>SS-SLIGHTY STICKY                 |  |
| FS-FOOT SLOPE<br>N-NOSE SLOPE<br>H-HEAD SLOPE             | II           | SL-SANDY LOAM<br>L-LOAM   | 0.8 - 0.6          | FI-FIRM<br>VFI-VERY FIRM<br>EFI-EXTREMELY FIRM | S-STICKY<br>VS-VERY STICKY<br>NP-NON-PLASTIC       |  |
| CC-CONCLAVE SLOPE CV-CONVEX SLOPE T-TERRACE FP-FLOOD PLAN | III          | SI-SILT<br>SIL-SILT LOAM<br>CL-CLAY LOAM<br>SCL-SANDY CLAY LOAM | 0.6 - 0.3          |  | SP-SLIGHTLY STICKY<br>P-PLASTIC<br>VP-VERY PLASTIC |  |

0.4 - 0.1

IV SIC-SILTY CLAY C-CLAY

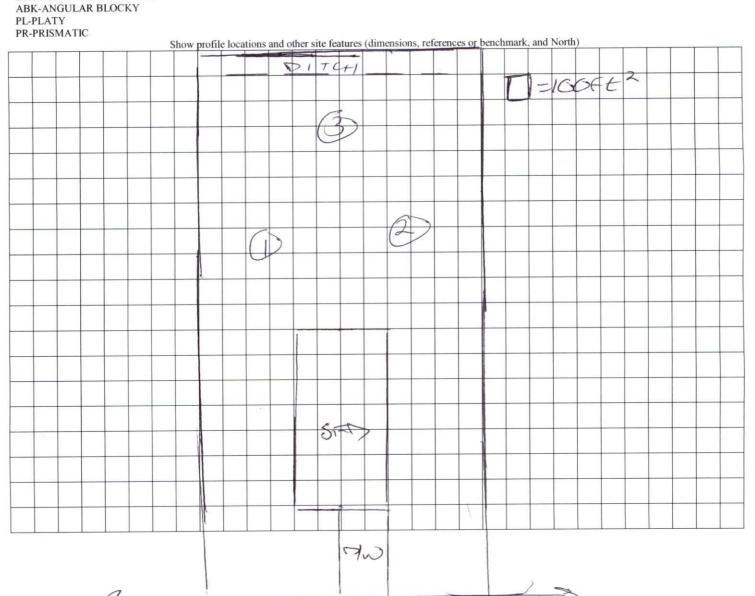
SC-SANDY CLAY

STRUCTURE
SG-SINGLE GRAIN
M- MASSIVE
CR-CRUMB
GR-GRANULAR
SBK-SUBANGULAR BLOCKY

MINERALOGY SLIGHTLY EXPANSIVE

EXPANSIVE

EALWIN



WALKER GRENTE LD.