



BLUE RAVEN SOLAR, LLC.  
Firm License No. D-0449  
1403 North Research Way , Bldg. J  
Orem, UT 84097

January 17, 2025

To: Blue Raven Solar  
1403 North Research Way, Building J  
Orem, UT. 84097

Subject: Certification Letter  
Haynes Residence  
125 Hungry Creek Dr  
Linden, NC. 28356

To Whom It May Concern,

A jobsite observation of the condition of the existing framing system was performed by an audit team of Blue Raven Solar. All review is based on these observations and the design criteria listed below and only deemed valid if provided information is true and accurate.

On the above referenced project, the roof structural framing has been reviewed for additional loading due to the installation of the solar PV addition to the roof. The structural review only applies to the section of the roof that is directly supporting the solar PV system and its supporting elements. The observed roof framing is described below. If field conditions differ, contractor to notify engineer prior to starting construction.

The roof structure of (MP1) consists of composition shingle on roof plywood that is supported by pre-manufactured trusses that are spaced at @ 24" o.c.. The top chords, sloped at 30 degrees, are 2x4 sections, the bottom chords are 2x4 sections and the web members are 2x4 sections. The truss members are connected by steel gusset plates. The max unsupported projected horizontal top chord span is approximately 7'-4".

The existing roof framing system of (MP1) is judged to be adequate to withstand the loading imposed by the installation of the solar panels. No reinforcement is necessary.

The spacing of the solar standoffs should be kept at 72" o.c. for landscape and 48" o.c. for portrait orientation, with a staggered pattern to ensure proper distribution of loads.

The scope of this report is strictly limited to an evaluation of the fastener attachment, underlying framing and supporting structure only. The attachment's to the existing structure are required to be in a staggered pattern to ensure proper distribution of loading. All panels, racking and hardware shall be installed per manufacturer specifications and within specified design limitations. All waterproofing shall be provided by the manufacturer.

Note: Seismic check is not required since  $S_s < .4g$  and Seismic Design Category (SDC) < B

Design Criteria:

- Applicable Codes = 2018 North Carolina State Building Code (NCSBC), ASCE 7-10
- Roof Dead Load = 7 psf (MP1)
- Roof Live Load = 20 psf
- Wind Speed = 115 mph (Vult), Exposure C, Risk Category II
- Ground Snow Load = 15 psf - Roof Snow Load = 10.5 psf
- Attachment: 2 - #14 Wood Screws with 2.5 inch min. embedment depth, at spacing shown above.

Please contact me with any further questions or concerns regarding this project.

Sincerely,

John Calvert, P.E.  
Project Engineer



Digitally signed by  
John A. Calvert  
Date: 2025.01.17  
10:28:31 -07'00'  
Haynes Linden NC 1



### Gravity Loading

| Roof Snow Load Calculations                       |                 |                     |
|---|-----------------|---------------------|
| $p_g$ = Ground Snow Load =                        | 15 psf          |                     |
| $p_f = 0.7 C_e C_t I p_g$                         |                 | (ASCE7 - Eq 7-1)    |
| $C_e$ = Exposure Factor =                         | 1               | (ASCE7 - Table 7-2) |
| $C_t$ = Thermal Factor =                          | 1               | (ASCE7 - Table 7-3) |
| $I$ = Importance Factor =                         | 1               |                     |
| $p_f$ = Flat Roof Snow Load =                     | 10.5 psf        |                     |
| $p_s = C_s p_f$                                   |                 | (ASCE7 - Eq 7-2)    |
| $C_s$ = Slope Factor =                            | 1               |                     |
| <b><math>p_s</math> = Sloped Roof Snow Load =</b> | <b>10.5 psf</b> |                     |

| PV Dead Load = 3 psf (Per Blue Raven Solar)                               |              |
|---|--------------|
| DL Adjusted to 30 Degree Slope  | 3.46 psf     |
| PV System Weight  |              |
| Weight of PV System (Per Blue Raven Solar)                                | 3.0 psf      |
| X Standoff Spacing =  | 4.00 ft      |
| Y Standoff Spacing =  | 3.04 ft      |
| Standoff Tributary Area =   | 12.17 sft    |
| <b>Point Loads of Standoffs</b>   | <b>37 lb</b> |
| Note: PV standoffs are staggered to ensure proper distribution of loading |              |

| Roof Live Load = 20 psf  |  |
|--|--|
| Note: Roof live load is removed in area's covered by PV array. |  |

| Roof Dead Load (MP1)           |                |                       |
|--------------------------------|----------------|-----------------------|
| Composition Shingle            | 4.00           |                       |
| Roof Plywood                   | 2.00           |                       |
| 2x4 Top Chords @ 24"o.c.       | 0.73           |                       |
| Vaulted Ceiling                | 0.00           | (Ceiling Not Vaulted) |
| Miscellaneous                  | 0.27           |                       |
| <b>Total Roof DL (MP1)</b>     | <b>7.0 psf</b> |                       |
| DL Adjusted to 30 Degree Slope | 8.1 psf        |                       |



## Wind Calculations

### Per ASCE 7-10 Components and Cladding

| Input Variables     |            |
|---------------------|------------|
| Wind Speed          | 115 mph    |
| Exposure Category   | C          |
| Roof Shape          | Hip/Gable  |
| Roof Slope          | 30 degrees |
| Mean Roof Height    | 20 ft      |
| Effective Wind Area | 21.3 ft    |

| Design Wind Pressure Calculations                          |                |
|--|----------------|
| <b>Wind Pressure <math>P = qh \cdot G \cdot C_n</math></b> |                |
| $qh = 0.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V^2$  | (Eq. 30.3-1)   |
| $K_z$ (Exposure Coefficient) = 0.9                         | (Table 30.3-1) |
| $K_{zt}$ (topographic factor) = 1                          | (Fig. 26.8-1)  |
| $K_d$ (Wind Directionality Factor) = 0.85                  | (Table 26.6-1) |
| $V$ (Design Wind Speed) = 115 mph                          | (Fig. 26.5-1A) |
| Risk Category = II   | (Table 1.5-1)  |
| $qh = 25.90$   |                |
| $0.6 \cdot qh = 15.54$                                     |                |

| Standoff Uplift Calculations-Portrait |                |                |                |          |
|---------------------------------------|----------------|----------------|----------------|----------|
|                                       | Zone 1         | Zone 2         | Zone 3         | Positive |
| $GC_p =$                              | -0.94          | -1.15          | -1.15          | 0.86     |
| Uplift Pressure =                     | -14.55 psf     | -17.80 psf     | -17.80 psf     | 22.4 psf |
| X Standoff Spacing =                  | 4.00           | 4.00           | 2.67           |          |
| Y Standoff Spacing =                  | 3.04           | 3.041666667    | 3.041666667    |          |
| Tributary Area =                      | 12.17          | 12.17          | 8.11           |          |
| Dead Load on Attachment=              | 36.50          | 36.50          | 24.33          |          |
| <b>Footing Uplift (0.6D+0.6W)=</b>    | <b>-155 lb</b> | <b>-195 lb</b> | <b>-130 lb</b> |          |

| Standoff Uplift Calculations-Landscape |                |                |                |          |
|--|----------------|----------------|----------------|----------|
|  | Zone 1         | Zone 2         | Zone 3         | Positive |
| $GC_p =$                               | -0.94          | -1.15          | -1.15          | 0.86     |
| Uplift Pressure =                      | -14.55 psf     | -17.80 psf     | -17.80 psf     | 10.5 psf |
| X Standoff Spacing =                   | 6.00           | 6.00           | 4.00           |          |
| Y Standoff Spacing =                   | 1.75           | 1.75           | 1.75           |          |
| Tributary Area =                       | 10.50          | 10.50          | 7.00           |          |
| Dead Load on Attachment=               | 31.50          | 31.50          | 21.00          |          |
| <b>Footing Uplift (0.6D+0.6W) =</b>    | <b>-134 lb</b> | <b>-168 lb</b> | <b>-112 lb</b> |          |

| Standoff Uplift Check           |               |
|---------------------------------|---------------|
| Maximum Design Uplift =         | -195 lb       |
| Standoff Uplift Capacity =      | 400 lb        |
| 400 lb capacity > 195 lb demand | Therefore, OK |

| Fastener Capacity Check         |                     |
|---------------------------------|---------------------|
| Fastener =                      | 2 - #14 Wood Screws |
| Number of Fasteners =           | 2                   |
| Embedment Depth =               | 2.5                 |
| Pullout Capacity Per Inch =     | 150 lb              |
| Fastener Capacity =             | 750 lb              |
| w/ F.S. of 1.5 & DOL of 1.6=    | 800 lb              |
| 800 lb capacity > 195 lb demand | Therefore, OK       |

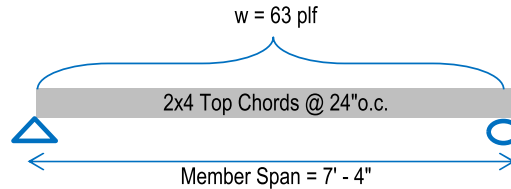


**Framing Check**  
**(MP1)**

**PASS**

Dead Load 8.1 psf  
PV Load 3.5 psf  
Live Load 20.0 psf

Governing Load Combo = DL + LL  
**Total Load 31.5 psf**



| Member Properties |                      |                      |              |                |
|-------------------|----------------------|----------------------|--------------|----------------|
| Member Size       | S (in <sup>3</sup> ) | I (in <sup>4</sup> ) | Lumber Sp/Gr | Member Spacing |
| 2x4               | 3.06                 | 5.36                 | DF#2         | @ 24" o.c.     |

| Check Bending Stress                |                |   |                |   |                |   |                |
|-------------------------------------|----------------|---|----------------|---|----------------|---|----------------|
| Fb (psi) =                          | f <sub>b</sub> | x | C <sub>d</sub> | x | C <sub>f</sub> | x | C <sub>r</sub> |
|                                     | 900            | x | 1.25           | x | 1.5            | x | 1.15           |
| (NDS Table 4.3.1)                   |                |   |                |   |                |   |                |
| Allowed Bending Stress = 1940.6 psi |                |   |                |   |                |   |                |

Maximum Moment =  $(wL^2) / 8$   
 = 424.132 ft#  
 = 5089.584 in#  
 Actual Bending Stress = (Maximum Moment) / S  
 = 1662 psi

**Allowed > Actual -- 85.7% Stressed -- Therefore, OK**

| Check Deflection                  |                             |                           |
|-----------------------------------|-----------------------------|---------------------------|
| Allowed Deflection (Total Load) = | $L/180$                     | (E = 1600000 psi Per NDS) |
|                                   | = 0.488 in                  |                           |
| Deflection Criteria Based on =    | Continuous Span             |                           |
| Actual Deflection (Total Load) =  | $(w * L^4) / (185 * E * I)$ |                           |
|                                   | = 0.199 in                  |                           |
|                                   | = L/443 > L/180             | <b>Therefore OK</b>       |
| Allowed Deflection (Live Load) =  | $L/240$                     |                           |
|                                   | = 0.366 in                  |                           |
| Actual Deflection (Live Load) =   | $(w * L^4) / (185 * E * I)$ |                           |
|                                   | = 0.127 in                  |                           |
|                                   | = L/693 > L/240             | <b>Therefore OK</b>       |

| Check Shear                                 |                                |                |
|---|--------------------------------|----------------|
| Member Area = 5.3 in <sup>2</sup>           | F <sub>v</sub> (psi) = 180 psi | (NDS Table 4A) |
| Allowed Shear = F <sub>v</sub> * A = 945 lb | Max Shear (V) = w * L / 2 =    | 231 lb         |

**Allowed > Actual -- 24.5% Stressed -- Therefore, OK**