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STRUCTURAL ANALYSIS for the ROOFTOP PV SOLAR INSTALLATION

Project: Chong Ting, 66 Pecan Grv Ln, Fuquay Varina, NC 27526

Prepared for:

EMPWR Solar

1007 Johnnie Dodds Blvd Suite 111 - Charleston, SC 29464

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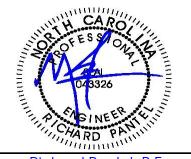
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Project No: 66.414408.86, Rev. 0 Report Date: 02/26/2025 Report Prepared by:



Richard Pantel, P.E. NC License No. 43326 Sealed 02/26/2025

Loading Summary

ĺ	Exposure and Occupancy Categories								
B Exposure Category (ASCE 7-10 Table 26.7.3, Page 274)									
ĺ	П		Building Use Occupancy / Risk Category (ASCE 7-10 Table 1.5-1, Page 5)						

	Wind Loading:								
V	117	mph	ASCE 7-10, Figure 26.5-1 A, B or C, pp 249-251. [(117 mph, 50						
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		Πρπ	year wind MRI)]						
qz	20.82	psf	Velocity qz, calculated at height z [ASD]						

Snow Loading						
pg	15.00	psf	Ground Snow Load pg (ASCE 7-10 Table 7.2-1, Page 56-60)			
Total Snow I	Load					
ps	15.00	psf	Effective snow load on roof and modules			

Module Data								
Jinko Sola	Jinko Solar: JKM425N-54HL4-B							
Dimensions	mm	ft	in					
Length	1,722	5.65	67.80					
Width	1,134	3.72	44.65					
Area (m^2, ft^2)	2.0	21.02						
Weight	kg	lb						
Module	22.00	48.50						

Roof Panel (Cladding) Loading Sum	Module Loading Summary				
Support Point Loads		Upward	Upward	Upward	Downward
Roof Zones		1	2	3	All
Net load per module	lb	-35	-150	-298	171

Positive values indicate net downward force

Primary Stanchion: IronRidge HALO ULTRAGRIP - (QM-HUG-01-B1)

StanchionFastener Pull-ou					
Framing spacing	ft	2.00	<u> </u>		l
Rails / Module	ea	2	1		
Max proposed stanchion span	ft	4.00	1		
# fasteners per stanchion		2	1		
Bolt thread embedment depth	in	1.75	1		
Safety Factor		1.10	1		
Pull-out for #14 threaded fasteners	lb/in	134	lb per inch	of embedm	ent
Factored max fastener uplift capacity	lb	425	1		
Fastener details Material Stainless	Size	#14	Predrill hol	e 0.12" dia (or use self tapping
Max stanchion uplift capacity	lb	1100	1		,, 0
Max support point uplift capacity	lb	425	1		
, , , , , ,		•	•		
Roof Zones		1	2	3	
Net lift per module	lb	35	150	298	
Min tot bolt thread embedment depth rq'd	in	0.15	0.62	1.23	
Net uplift pressure 7. 0.6D - 0.6W	psf	-1.56	-6.64	-13.21	
Allowable lift area / support point	sf	271.70	63.97	32.16	
Max rail span per support spacing	ft	4.00	4.00	4.00	
Landscape Modules			_		-
Length along rafter	ft	3.72			_
Lift calc'ed max stanchion EW spacing	ft	> 6	> 6	> 6	
Max stanchion EW spacing	ft	4.00	4.00	4.00	
Maximum module area / support point	sf	7.44	7.44	7.44	
Factored lift per support point	lb	-12	-49	-98	
Portrait Modules			_		
Length along rafter	ft	5.65			-
Lift calc'ed max stanchion EW spacing	ft	> 6	> 6	> 6	
Max stanchion EW spacing	ft	4.00	4.00	4.00	
Maximum module area / support point	sf	11.30	11.30	11.30	
Factored lift per support point	lb	-18	-75	-149	

Stanchion support threaded fastener sizes are indicated in the Module Loading Summary table above. Lift forces were determined from GCp and other coefficients contained in the ASCE nomographs

Conclusions

We were asked to review the roof of Chong Ting, located at 66 Pecan Grv Ln, Fuquay Varina, NC, by EMPWR Solar, to determine its suitability to support a PV solar system installation.

The referenced building's roof structure was field measured by EMPWR Solar. The attached framing analyses reflect the results of those field measurements combined with the PV solar module locations shown on the PV solar roof layout design prepared by EMPWR Solar. Loads are calculated to combine the existing building and environmental loads with the proposed new PV array loads.

The IronRidge XR10 Rail racking and IronRidge HALO ULTRAGRIP - (QM-HUG-01-B1) stanchions were selected for this project by EMPWR Solar. The racking and support stanchions shall be placed as shown on their plans, dated 02/25/2025, and shall be fastened to the roof framing using fastener sizes indicated in this report. Rack support spacing shall be no more than that shown above. Note that support points for alternating rows shall share the same truss. Intermediate rows shall move the support points laterally to the next truss.



Google Location Map

Framing Summary

 Ex. Framing
 Total Ex DL

 MP 1: Truss @ 24" OC
 0.79 psf
 5.94 psf

Based upon the attached calculations, the existing roof's framing system is capable of supporting the additional loading for the proposed PV solar system along with the existing building and environmental loads. No supplemental roof framing structural supports are required. No further structural alterations or modifications are needed to support the system. Minimum required anchorage fastening is described above.

Wood fastener notes: 1) Fastener threads must be embedded in the side grain of a roof support structural member or other structural member integrated into the building's structure. 2) Fastener must be located in the middle third of the structural member. 3) Install fasteners with head and where required, washer, flush to material surface (no gap). Do not over-torque.

References and Codes:

- 1) ASCE 7-10 Minimum Design Loads for Buildings and Other Structures
- 2) 2015 IBC
- 3) 2018 NC Building Code
- 4) American Wood Council, NDS 2018, Table 12.2A, 12.3.3A.
- 5) American Wood Council, Wood Structural Design, 1992, Figure 6.

^{*} Wood species used in these calculations assumes spruce, pine or fir, #2 grade.

Location: MP 1

Member: Truss - Total Length 24 ft, Unsupported 24 ft

Geometric Data						
Θ	deg.	25.0	Angle of roof plane from horizontal, in degrees			
ω	deg.	0.0	Angle the solar panel makes with the roof surface			
L	ft.	42.00	Length of roof plane, in feet (meters)			
W	ft.	22.58	Plan view width of roof plane, in feet (meters)			
h	ft.	24.46	Average height of roof above grade, in feet (meters)			

Roof Wind Zone Width						
	use, a =	3.00	ft			

Wind Velocity Pressure, q_z evaluated at the height z									
$q_z =$	q_z = 20.82 psf Vasd q_z = 12.61 psf Basic wind pressure								
V=	117	mph							

Framing Data						
Wood type	US Spruce					
Wood source, moisture content	White 0.12%					
# Framing Members / Support		1				
Rafter / Truss OC	in	24.00				
Member Total Length	ft	24.00				

2 # Rafters / Rack Support Width			
4.00	Rack Support Spacing (ft)		
48.00	Max. Rack Support Spacing (in)		
3	Max # of mod's / Truss top chord		

Member Properties	Member
Name	(1) 2x4
Repetitive Member Factor (Cr)	1.15

* Mem properties based upon field measurements

Truss top chord

Module Data						
Weight kg lb psf load						
Module	22.00	48.50	2.31			
4 Stanchions	0.91	2.0	0.10			

Existing Dead Loads	Units	Value	Description
Roof Deck & Surface Material*	psf	5.15	Truss members' self weight added to FEA analysis
	_		* Roof surface: Shingles, Asphalt, Architectural (Typic

Rack Support Spacing	and Loadir	ng			
Across rafters	ft	4.0			
Along rafter slope	ft	5.6			
Area / support point	sf	11.3			
Uphill gap between modules	in	1.0	0.08	ft	

Member To	otal Length	ft	24.00		
Maximum member free span		ft	24.00	Truss top cho	ord span
	Zones	1	2	3	
	GCp	-0.87	-1.54	-2.41	

Downward, Zones 1, 2 & 3
GCp 0.44

ASCE 7-10 Chapter 2 Combinations of Loads, Table 2.4, Page 8 (in psf)						
Zones	1	2	3	1, 2 & 3		
2.2 SYMBOLS AND NOTATION		Module	Module	Downward		
		Upward	Upward	Downward		
D = dead load of PV Module + Stanchion	2.40	2.40	2.40	2.40		
S = snow load	15.00	15.00	15.00	15.00		
W = wind load = (Vu Windload) = (Vasd Windload / 0.6)	-10.95	-19.41	-30.35	5.49		

2.4 Combining Nominal Loads Using Allowable Stress Design (in psf)

2.4.1 Basic Combinations. Loads listed herein shall be considered to act in the following combinations; whichever produces the most unfavorable effect in the building, foundation, or structural member being considered. Effects of one or more loads not acting shall be considered.

Combination Formulae	Upward	Upward	Upward	Downward
Use this loading combination for DOWNWARD for Proposed PV Dead Load				
3. D + S	17.40	17.40	17.40	17.40
Module Support point load (lb)	197	197	197	197
Cr Factored Module Support point load (lb)	171	171	171	171

Use this loading combination for UPWARD for Proposed PV Dead Load						
7. 0.6D - 0.6W -1.56 -6.64 -13.21 5.00						
Module Support point load (lb) -18 -75 -149 57						

DOWNWARD

Presume loading directly over member.

	Combined Dead and Wind Pressure Downward Loading					
	Trus	s top chord	span			
PV Module Row	Point load loc's from Left support	Point Load #'s	Module Support Point Load	Comment	Module Orientation	
	ft from left		lb			
1	0.84		171		Portrait	
1	6.49			Support placed on adjoining truss	Portrait	
2	6.57			Support placed on adjoining truss	Portrait	
2	12.22		171		Portrait	
3	12.31		171		Portrait	
3	17.96			Support placed on adjoining truss	Portrait	

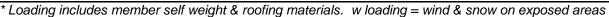
Truss Data and Loading for MP 1

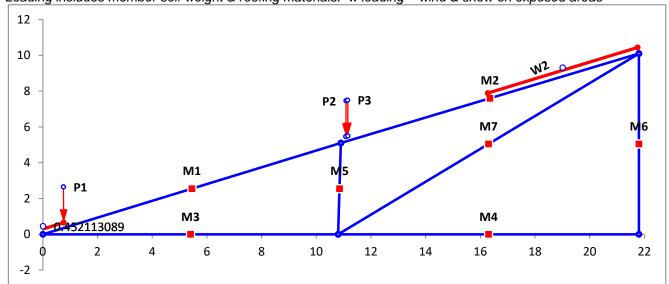
Roof slope (degrees)	25.00
Top ridge height above floor plane	10.14

Length of roof plane	24.00
Length of floor plane	21.75

			I I	ľ
Roof	Plane	lane Floor Plar		
Mem #	Mem Type	Mem #	Мет Туре	
1	2x4	3	2x4	
2	2x4	4	2x4	

russ Segments							
	Diago	onals	Diag	onals			
	Mem #	Mem Type	Mem #	Мет Туре			
	5	2x4	7	2x4			
	6	2x4					





Snow Loading Analysis

where:

Fully Exposed Exposure category Exposure Factor, Ce (ASCE 7-10 Table 7.3-1, Page 61) Ce 0.9 Thermal Factor, Ct (ASCE 7-10 Table 7.3-2, Page 61) Ct 1.0 ls 1.0 Snow Importance Factor, Is (ASCE 7-10 Table 1.5-2, Page 5) Ground Snow Load pg (ASCE 7-10 Table 7.2-1, Page 56-60) 15.00 p_g 0.7CeCtIsPg Flat Roof Snow Load, pf (ASCE 7-10 Table 7.3-1, Page 61) 9.45 but where Pf is not less than the following: Minimum Snow Load pm (ASCE 7-10 Table 7.3.4, Page 62) 15.00 When $Pg \le 20 psf$, then use Pf = Pg x Is p_{m} 15.00 psf. Resultant Snow pressure to be used with Roof slope factor below Sloped Roof Snow Load ps (ASCE 7-10 Table 7.4, Page 61) p_s C_sp_f Roof Type Warm Roofs Roof slope factor Cs for Warm Roofs, where Ct = 1.0

Roof surface condition = Slippery Roof

Roof Slope Factor, Cs (ASCE 7-10 Table 7.4-1a, Page 62) $C_s =$

Total Snow Load

15.00 psf Roof snow load p_s =

FEA Calculation Results for Roof Plane MP 1 for EMPWR Solar Client CHONG TING

IDSPL - 2D Frame Analysis of a 2D frame subject to distributed loads, point loads and moments

Equilibrium check	FX	FY	
Total applied forces	0.00	2047	
Total output reactions	0.00	-2047	
Output error	6.73E-13	-6.82E-13	

0.00054		Shear	Ax
	Max (psi)	6	241
	Allowable (psi)	115	5,610

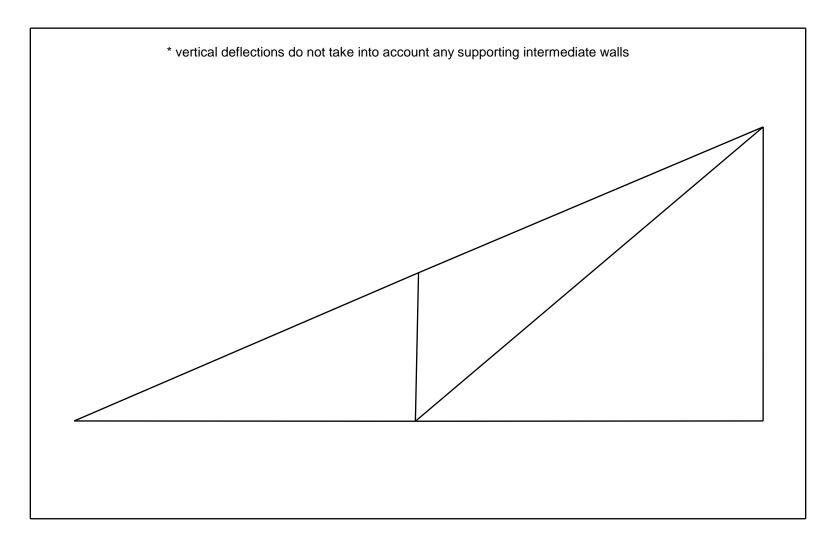
of segments/beam

Maximum Deflections				
-1.66E-03	-5.38E-03			

_	Node Re	esults		Beam End Results		
Direction	Deflection	Reaction	Beam	Shear Axial		BM
DX1	0.00E+00	0	1-1	-148	695	0
DY1	0.00E+00	-782	1-2	196	534	0
RZ1	0.00E+00	0	2-1	-235	742	0
DX2	-1.63E-03	0	2-2	775	279	0
DY2	5.38E-03	0	3-1	-353	-567	0
RZ2	0.00E+00	0	3-2	-2	-567	0
DX3	1.11E-03	0	4-1	0	0	0
DY3	1.34E-03	0	4-2	0	0	0
RZ3	0.00E+00	0	5-1	0	492	0
DX4	-6.51E-04	0	5-2	0	474	0
DY4	5.10E-03	0	6-1	0	1266	0
RZ4	0.00E+00	0	6-2	0	1205	0
DX5	-6.51E-04	0	7-1	-29	-756	0
DY5	0.00E+00	-1266	7-2	64	-841	0
RZ5	0.00E+00	0				
Rel1-3	4.82E-04	0				
Rel1-6	1.03E-03	0				

* vertical deflections	s do not take into	account any su	pporting intermediate v	valls

Beam	Χ	Shear	Mom	Axial	DX	DY	RZ
1	0.00	-148	0	695	0.00E+00	0.00E+00	0.00E+00
1	12.03	93	620	582	-1.66E-03	-5.37E-03	6.80E-04
2	0.00	-235	0	742	-1.63E-03	-5.38E-03	0.00E+00
2	11.99	333	6754	481	8.11E-04	-1.20E-03	1.43E-04
3	0.00	-353	0	-567	0.00E+00	0.00E+00	0.00E+00
3	10.80	-103	612	-567	-6.51E-04	-5.10E-03	6.34E-04
4	0.00	0	0	0	-6.51E-04	-5.10E-03	0.00E+00
4	11.00	0	0	0	-6.51E-04	0.00E+00	-4.63E-04
5	0.00	0	0	492	-6.51E-04	-5.10E-03	0.00E+00
5	5.10	0	0	479	-1.63E-03	-5.38E-03	1.94E-04
6	0.00	0	0	1266	-6.51E-04	0.00E+00	0.00E+00
6	10.10	0	0	1214	1.11E-03	-1.34E-03	-1.74E-04
7	0.00	-29	0	-756	-6.51E-04	-5.10E-03	0.00E+00
7	14.93	53	5	-832	1.11E-03	-1.34E-03	-3.46E-04
·							
·							



Scaled 2X Deflected Truss Plot
Roof Plane MP 1 for EMPWR Solar Client CHONG TING