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STRUCTURAL ANALYSIS for the ROOFTOP PV SOLAR INSTALLATION

Project: Lee Osterhout, 42 Oakland Drive Sanford Nc 27332, Sanford, NC 27332

Prepared for:



Freedom Solar, LLC 4801 Freidrich Ln, Ste 100 - Austin, TX 78744

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Project Number: 36.114630, Rev. 0

Report Date: 06/03/2024

Report Prepared by:



Richard Pantel, P.E. NC License No. 43326 Sealed 06/03/2024

v405222 Richard Pante dnQualifier=A01410C0000018E57987 26E0001A3B4, cn=Richard Pantel ID.I 1W7 Cover

Digitally signed by Richard Pantel DN: c=US, o=TECTONICORP PC, Date: 2024.06.03 17:06:55 -04'00'

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Loading Summary

Exposure and Occupancy Categories					
В	B Exposure Category (ASCE 7-10 Table 26.7.3, Page 266)				
	Building Use Occupancy / Risk Category (ASCE 7-10 Table 1.5-1, Page 4)				

	Wind Loading:								
v	117	mph	ASCE 7-10, Figure 26.5-1 A, B or C, pp 249-251. [(117 mph, 50						
v	117	тірп	year wind MRI)]						
qz	20.76	psf	Velocity qz, calculated at height z [ASD]						

	Snow Loading							
pg	pg 10.00 psf Ground Snow Load pg (ASCE 7-10 Table 7.2-1, Page 52-53)							
Total Snow	Total Snow Load							
ps	ps 10.00 psf Effective snow load on roof and modules							

Module Data							
Mission Solar: MSE395SX9R							
Dimensions mm ft in							
Length	1,907	6.26	75.08				
Width	Width 1,054 3.46 41.50						
Area (m^2, ft^2)	2.0	21.64					
Weight	kg	lb					
Module	22.00	48.50					

Roof Panel (Cladding) Loading Sum	Module Loading Summary				
Support Point Loads		Upward	Upward	Upward	Downward
Roof Zones		1	2	3	All
Net load per module	lb	-271	-366	-366	295

Positive values indicate net downward force

Stand	chion Faste	ner Pull-ou	t and Space	cing Calcul	ations
Framing spacing			ft	2.00	
Rails / Module			ea	2	
Max proposed stanchi	on span		ft	6.00	
# fasteners per stanchion				1]
Bolt thread embedment depth			in	3	
Safety Factor				1.10	
Pull-out for 5/16 thread	ded fastene	rs	lb/in	220	
Factored max fastene	r uplift capa	city	lb	599	
Fastener details	Material	Stainless	Size	5/16	Predrill hole 0.16" dia or use self ta
Max stanchion uplift capacity			lb	618	
Max support point uplift capacity			lb	599	

Roof Zones		1	2	3	
Net lift per module	lb	271	366	366	
Min tot bolt thread em	bedment depth rq'd	in	1.36	1.83	1.83
Net uplift pressure	et uplift pressure 7. 0.6D - 0.6W			-9.75	-9.75
Allowable lift area / su	pport point	sf	82.85	61.42	61.42
Max rail span per fram	ing spacing	ft	6.00	6.00	6.00
Landscape Modules					
Length along rafter	ft	3.46			
Lift calc'ed max stand	ft	> 6	> 6	> 6	
Max stanchion EW spacing		ft	6.00	6.00	6.00
Maximum module are	sf	10.37	10.37	10.37	
Factored lift per supp	ort point	lb	-75	-101	-101
Portrait Modules				_	
Length along rafter		ft	6.26		
Lift calc'ed max stanchion EW spacing		ft	> 6	> 6	> 6
Max stanchion EW spacing		ft	6.00	6.00	6.00
Maximum module are	sf	18.77	18.77	18.77	
Factored lift per supp	ort point	lb	-136	-183	-183

Stanchion support threaded fastener sizes are indicated in the Module Loading Summary table above. Lift forces were determined from GCp and other coefficients contained in the ASCE nomographs

Conclusions

We were asked to review the roof of Lee Osterhout, located at 42 Oakland Drive Sanford Nc 27332, Sanford, NC, by Freedom Solar, LLC, to determine its suitability to support a PV solar system installation.

The referenced building's roof structure was field measured by Freedom Solar, LLC on 05/16/2024. The attached framing analyses reflect the results of those field measurements combined with the PV solar module locations shown on the PV solar roof layout design prepared by Freedom Solar, LLC. Loads are calculated to combine the existing building and environmental loads with the proposed new PV array loads.

The Pegasus PSR-B Rail racking and Pegasus Solar InstaFlash PIF-RB0 stanchions were selected for this project by Freedom Solar, LLC. The racking and support stanchions shall be placed as shown on their plans, dated 06/03/2024, and shall be fastened to the roof framing using fastener sizes indicated in this report. Rack support spacing shall be no more than that shown above. Note that support points for alternating rows shall share the same truss. Intermediate rows shall move the support points laterally to the next truss. The support rail can be cantilevered up to 1/3 of the maximum span between modules. 1/3 maximum span = 24.00 inches.



Framing Summary

	<u>Ex. Framing</u>	<u>Total Ex DL</u>
MP 1: Truss @ 24" OC	0.79 psf	5.19 psf
MP 2: Truss @ 24" OC	0.79 psf	5.19 psf
* Manual and a standard for the second standard for a second second second second second second second second s		

* Wood species used in these calculations assumes spruce, pine or fir, #2 grade.

Based upon the attached calculations, the existing roofs' framing systems are capable of supporting the additional loading for the proposed PV solar system along with the existing building and environmental loads. No supplemental roof framing structural supports are required. Minimum required anchorage fastening is described above.

Wood fastener notes: 1) Fastener threads must be embedded in the side grain of a roof support structural member or other structural member integrated into the building's structure. 2) Fastener must be located in the middle third of the structural member. 3) Install fasteners with head and where required, washer, flush to material surface (no gap). Do not over-torque.

References and Codes:

- 1) ASCE 7-10 Minimum Design Loads for Buildings and Other Structures
- 2) 2015 IBC
- 3) 2018 NC Building Code
- 4) American Wood Council, NDS 2018, Table 12.2A, 12.3.3A.
- 5) American Wood Council, Wood Structural Design, 1992, Figure 6.

Roof Structural Calculations for PV Solar Installation Location: MP 1 Member: Truss - Total Length 22.5 ft, Unsupported 22.5 ft

Geometric Data								
θ	deg.	34.00	Angle of roo	of plane froi	m horizontal, in degrees			
ω	deg.	0.00	Angle the s	olar panel r	nakes with the roof surface			
L	ft.	28.00			n feet (meters)			
W	ft.	18.50	Plan view width of roof plane, in feet (meters)					
h	ft.	18.67	Average he	ight of roof	above grade, in feet (meters)			
			-					
Roof Wind Zone			4					
use, a =	3.00	ft	J					
	- (- 1 - (1 - 1							
Wind Velocity Pressure, q_z evaluated		_						
q _z = 20.76 psf	Vasd q _z =	12.61	psf	Basic win	d pressure			
V= 117			n	nph				
Framing Da			4					
Wood type		pruce	-					
Wood source, moisture content	vvnite	0.12%	-	3	# Rafters / Rack Support Width			
# Framing Members / Support Rafter / Truss OC	in	1	4	6.00	Rack Support Spacing (ft)			
Member Total Length	in ft	24.00 22.50	-	72 3	Max. Rack Support Spacing (in) Max # of mod's / Truss top chord			
Member Total Length	п	22.50	1	3	Max # of filed's / Truss top chord			
Member Properties		Member	* Mem prop	erties base	d upon field measurements			
Name		(1) 2x4			op chord			
Repetitive Member Factor (Cr)		1.15	1		<u> </u>			
			-					
Module P	hysical Data	3						
Weight	kg	lb	psf load					
Module	22.00	48.50	2.24					
4 Stanchions	1.36	3.0	0.14					
Existing Dead Loads	Units	Value			cription			
Roof Deck & Surface	psf	4.40	Truss mem	bers' self w	eight added to FEA analysis			
Deels Comment Conseins			1					
Rack Support Spacing Across rafters		ig 6.0	4					
	ft ft	6.3	4					
Along rafter slope	sf	18.8	4					
Area / support point Uphill gap between modules	in	1.0	0.08	ft	1			
Lobum Sab permeen modules		1.0	0.00	1,1	1			
Member Total Length	ft	22.50			7			
Maximum member free span	ft	22.50	Truss top che	ord span	1			
Zones		2	3		J Downward, Zones 1, 2 & 3			
GCp		-1.13	-1.13	1	GCp 0.87			
<u> </u>				-4				

ASCE 7-10 Chapter 2 Combinations of Loads, Table 2.4, Page 8 (in psf)							
Zones	1	2	3	1,2&3			
2.2 SYMBOLS AND NOTATION	Module	Module	Module	Downward			
2.2 STRIBULS AND NOTATION		Upward	Upward	Downwaru			
D = dead load of PV Module + Stanchion	2.38	2.38	2.38	2.38			
S = snow load	10.00	10.00	10.00	10.00			
W = wind load = (Vu Windload) = (Vasd Windload / 0.6)	-19.61	-23.82	-23.82	18.22			

2.4 Combining Nominal Loads Using Allowable Stress Design (in psf)

2.4.1 Basic Combinations. Loads listed herein shall be considered to act in the following combinations; whichever produces the most unfavorable effect in the building, foundation, or structural member being considered. Effects of one or more loads not acting shall be considered.

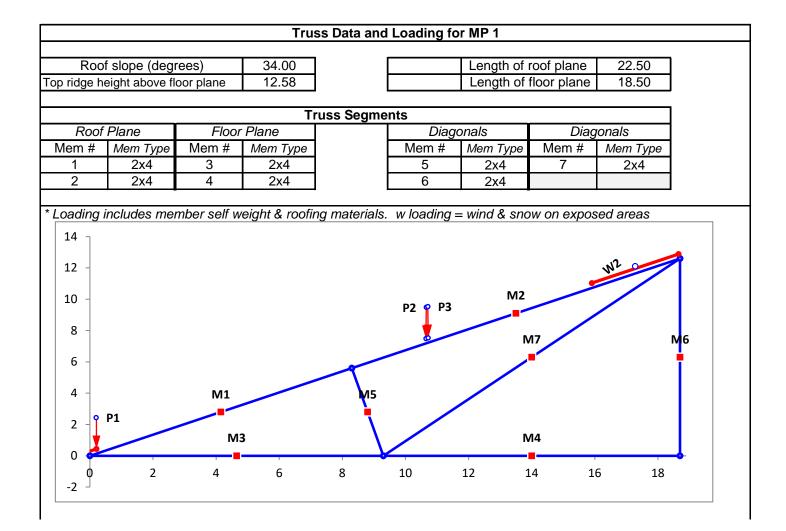
Combination Formulae	Upward	Upward	Upward	Downward		
Use this loading combination for DOWNWARD for Proposed PV Dead Load						
6. D + 0.75L - 0.75(0 or 0.7)eE + 0.75S	12.38	12.38	12.38	18.08		
Module Support point load (lb)	232	232	232	339		
Cr Factored Module Support point load (lb)	202	202	202	295		

Use this loading combination for UPWARD for Proposed PV Dead Load												
7. 0.6D - 0.6W	-7.23	-9.75	-9.75	4.54								
Module Support point load (lb)	-136	-183	-183	85								

DOWNWARD

Presume loading directly over member.

	Combined Dead and Wind Pressure Downward Loading												
	Trus	s top chord	span										
PV Module Row	e loc's from Point Sup		Module Support Point Load	Comment	Module Orientation								
	ft from left		lb										
1	0.25		295		Portrait								
1	6.51			Support placed on adjoining truss	Portrait								
2	6.59			Support placed on adjoining truss	Portrait								
2	12.85		295		Portrait								
3	12.93		295		Portrait								
3	19.19			Support placed on adjoining truss	Portrait								



Roof Structural Calculations for PV Solar Installation Location: MP 2 Member: Truss - Total Length 11 ft, Unsupported 11 ft

			Geom	etric Data						
	θ	deg.	34.00			m horizontal, in degrees				
	ω	deg.	0.00	Angle the s	olar panel r	nakes with the roof surface				
	L	ft.	24.00			n feet (meters)				
	W	ft.	9.00	Plan view width of roof plane, in feet (meters)						
	h	ft.	18.67	Average he	ight of roof	above grade, in feet (meters)				
	Roof Wind Zone		-							
	use, a =	3.00	ft	l						
	ressure, q _z evalua		eight z		1					
$q_z = 20$	0.76 <i>psf</i>	Vasd q _z =	12.61	psf	Basic win	d pressure				
V= 1	117			r	iph					
				-						
	Framing Da									
Wood type	_	US S								
	noisture content	White	0.12%		3	# Rafters / Rack Support Width				
# Framing Mem			1		6.00	Rack Support Spacing (ft)				
Rafter / Truss C	-	in	24.00		72	Max. Rack Support Spacing (in)				
Member Total L	ength	ft	11.00]	1	Max # of mod's / Truss top chord				
Member Prope	rties		Member	* Mem prop	erties hase	d upon field measurements				
Name			(1) 2x4			op chord				
Repetitive Mem	ber Factor (Cr)		1.15							
				4						
	Module P	hysical Data	3]					
W	eight	kg	lb	psf load	1					
	Module	22.00	48.50	2.24]					
	4 Stanchions	1.36	3.0	0.14						
Existing Dead	Loads	Units	Value		Desc	cription				
Roof Deck & Su	urface	psf	4.40	Truss mem	bers' self w	eight added to FEA analysis				
		<u> </u>		1						
	Support Spacing									
Across rafters		ft	6.0							
Along rafter slop		ft	6.3							
Area / support p		sf	18.8	0.00	<i>f</i> 4	7				
Uphill gap betw	een modules	in	1.0	0.08	ft	J				
Member Total L	ength	ft	11.00			1				
Maximum mem		ft	11.00	Truss top cho	ord span	1				
	Zones	1	2	3		J Downward, Zones 1, 2 & 3				
	GCp		-1.13	-1.13	1	GCp 0.87				
L	999				1	F				

ASCE 7-10 Chapter 2 Combinations of Loads, Table 2.4, Page 8 (in psf)													
Zones	1	2	3	1, 2 & 3									
2.2 SYMBOLS AND NOTATION	Module	Module	Module	Downward									
2.2 STMBOES AND NOTATION	Upward	Upward	Upward	Downward									
D = dead load of PV Module + Stanchion	2.38	2.38	2.38	2.38									
S = snow load	10.00	10.00	10.00	10.00									
W = wind load = (Vu Windload) = (Vasd Windload / 0.6)	-19.61	-23.82	-23.82	18.22									

2.4 Combining Nominal Loads Using Allowable Stress Design (in psf)

2.4.1 Basic Combinations. Loads listed herein shall be considered to act in the following combinations; whichever produces the most unfavorable effect in the building, foundation, or structural member being considered. Effects of one or more loads not acting shall be considered.

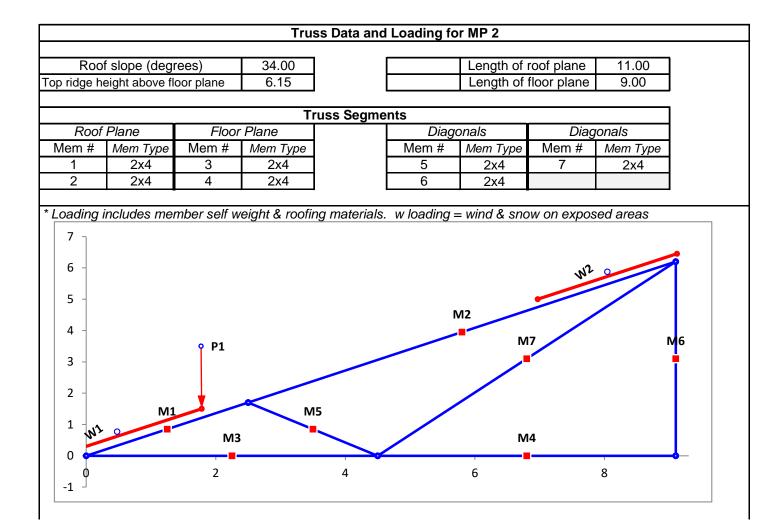
Combination Formulae	Upward	Upward	Upward	Downward								
Use this loading combination for DOWNWARD for Proposed PV Dead Load												
6. D + 0.75L - 0.75(0 or 0.7)eE + 0.75S	12.38	12.38	12.38	18.08								
Module Support point load (lb)	232	232	232	339								
Cr Factored Module Support point load (lb)	202	202	202	295								

Use this loading combination for UPWARD for Proposed PV Dead Load												
7. 0.6D - 0.6W	-7.23	-9.75	-9.75	4.54								
Module Support point load (lb)	-136	-183	-183	85								

DOWNWARD

Presume loading directly over member.

		Combined	Dead and	Wind Pressure Downward Loading	
	Trus	s top chord	span		
PV Module Row	Point load loc's from Left support	Point Load #'s	Module Support Point Load	Comment	Module Orientation
	ft from left		lb		
1	2.15		295		Portrait
1	8.41			Support placed on adjoining truss	Portrait



Snow Loading Analysis

where:

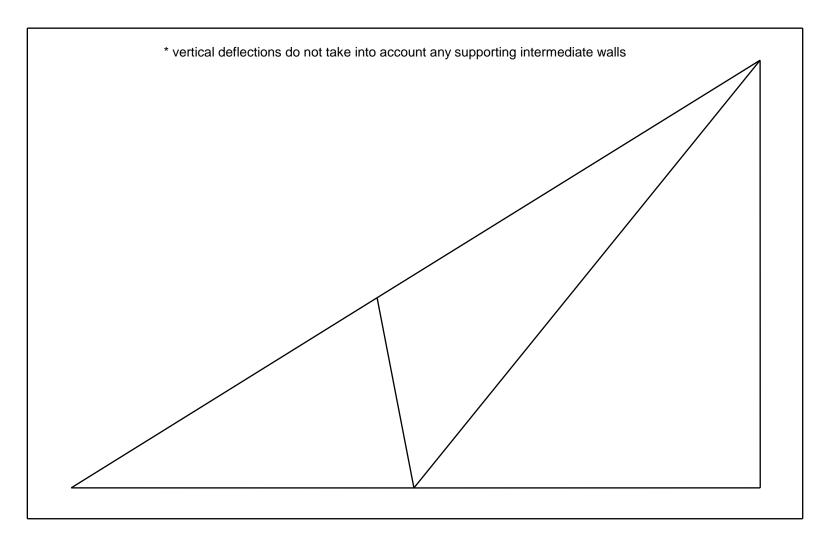
			Fully Exp	posed Exposure category
(Се	=	0.9	Exposure Factor, Ce (ASCE 7-10 Table 7.3-1, Page 58)
	Ct	=	1.0	Thermal Factor, Ct (ASCE 7-10 Table 7.3-2, Page 58)
	ls	=	1.0	Snow Importance Factor, Is (ASCE 7-10 Table 1.5-2, Page 5)
	p _g	=	10.00	Ground Snow Load pg (ASCE 7-10 Table 7.2-1, Page 52-53)
	p _f	=	0.7CeCt	IsPg Flat Roof Snow Load, pf (ASCE 7-10 Table 7.3-1, Page 58)
	p f	=	6.30	psf
				but where Pf is not less than the following:
				Minimum Snow Load pm (ASCE 7-10 Table 7.3.4, Page 53)
I	p _m	=	10.00	When $Pg \le 20 psf$, then use $Pf = Pg x Is$
	p _f	=	10.00	psf. Resultant Snow pressure to be used with Roof slope factor below
	p _s	=	C _s p _f	Sloped Roof Snow Load ps (ASCE 7-10 Table 7.4, Page 54)
	F 2		- 51-1	Roof Type Warm Roofs
Roof	slop	e fa	ctor Cs fo	or Warm Roofs, where $Ct = 1.0$
	•			Roof surface condition = Slippery Roof
	~		1.00	Deef Clane Factor, Co. (ACCE 7.10 Table 7.20, Dece 52)
	C _s	=	1.00	Roof Slope Factor, Cs (ASCE 7-10 Table 7-2a, Page 59)

Total Snow Load

p_s = **10.00 psf** Roof snow load

	Equilibriun	n check	FX	FY	0.00011					Shear	Mom	Ax			
	Total app	olied forces	0.00	2542				ſ	Max (psi)	1	11	178			
	Total outpu	ut reactions	0.00	-2542				Allowa	able (psi)	115	950	5,610	Maximum	Deflections	
	C	Output error	6.69E-13	-1.36E-12				#	of segme	ents/beam	1		-1.41E-03	-1.23E-03	
							_	* ve	rtical def	lections d	lo not take	into acco	unt any suppo	orting intermed	diate walls
_	Node Re	esults		Beam	n End Res	ults		Beam	Х	Shear	Mom	Axial	DX	DY	RZ
Direction	Deflection	Reaction	Beam	Shear	Axial	BM		1	0.00	-1258	5720	600	0.00E+00	0.00E+00	-4.01E-04
DX1	0.00E+00	0	1-1	-1258	600	5720		1	10.01	-958	-4125	398	-2.70E-04	-9.03E-04	-3.35E-04
DY1	0.00E+00	-1223	1-2	-890	352	-4480		2	0.00	-1369	-6927	-360	-2.57E-04	-9.12E-04	-1.63E-04
RZ1	-4.01E-04	0	2-1	-1369	-360	-6927		2	12.54	-634	-11459	-855	-1.41E-03	-1.05E-03	-2.55E-03
DX2	-2.57E-04	0	2-2	-194	-1151	-18430		3	0.00	155	-5720	206	0.00E+00	0.00E+00	-4.01E-04
DY2	9.12E-04	0	3-1	155	206	-5720		3	9.30	509	1664	206	1.30E-04	-9.16E-04	2.66E-04
RZ2	-1.63E-04	0	3-2	585	206	1268		4	0.00	-147	686	806	1.30E-04	-9.16E-04	-1.55E-04
DX3	-1.15E-03	0	4-1	-147	806	686		4	9.40	-147	-691	806	6.43E-04	0.00E+00	-1.70E-04
DY3	1.23E-03	0	4-2	-147	806	-691		5	0.00	-840	2337	172	1.30E-04	-9.16E-04	-1.55E-04
RZ3	1.33E-03	0	5-1	-840	172	2337		5	5.69	-843	-2448	155	-2.57E-04	-9.12E-04	-2.44E-04
DX4	1.30E-04	0	5-2	-844	150	-2447		6	0.00	806	-691	1466	6.43E-04	0.00E+00	-1.56E-04
DY4	9.16E-04	0	6-1	806	1466	-691		6	12.60	806	9461	1386	-1.15E-03	-1.23E-03	1.34E-03
RZ4	-1.55E-04	0	6-2	806	1374	9461		7	0.00	656	-1755	-449	1.30E-04	-9.16E-04	-1.55E-04
DX5	6.43E-04	0	7-1	656	-449	-1755		7	15.72	730	8974	-548	-1.15E-03	-1.23E-03	1.35E-03
DY5	0.00E+00	-1319	7-2	740	-561	8970									
RZ5	-1.56E-04	0]								
							1								

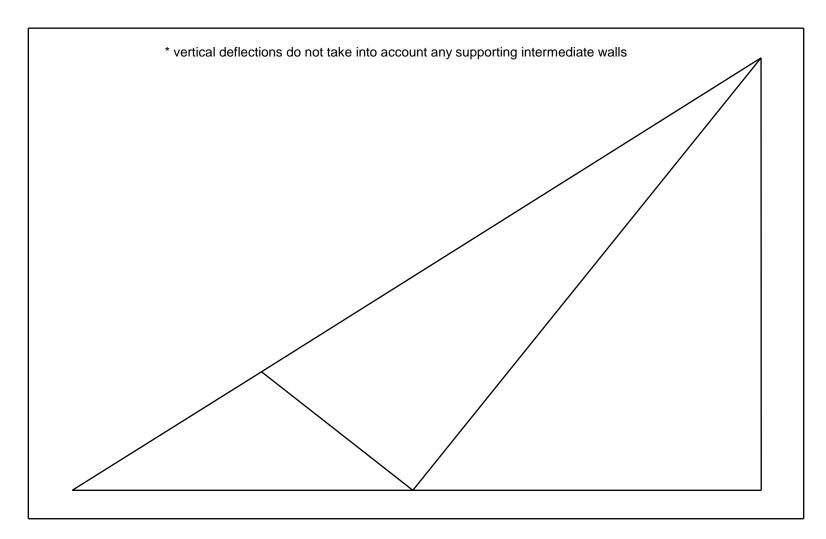
FEA Calculation Results for Roof Plane MP 1 for Freedom Solar, LLC Client Lee Osterhout IDSPL - 2D Frame Analysis of a 2D frame subject to distributed loads, point loads and moments



Scaled 2X Deflected Truss Plot Roof Plane MP 1 for Freedom Solar, LLC Client Lee Osterhout

	Equilibriun	n check	FX	FY	0.0001				Shear	Mom	Ax			
	Total app	olied forces	0.00	1101			P	Max (psi)	2	15	302			
	Total outpu	t reactions	0.00	-1101			Allowa	able (psi)	115	950	5,610	Maximum	Deflections	
	C	Output error	1.41E-12	-4.55E-13			#	of segme	ents/beam	1		-8.37E-04	-2.65E-04	
							* vei	rtical def	lections d	o not take	into acco	unt any suppo	orting intermed	liate walls
	Node Re	esults		Beam	n End Res	sults	Beam	Х	Shear	Mom	Axial	DX	DY	RZ
Direction	Deflection	Reaction	Beam	Shear	Axial	BM	1	0.00	-552	694	-208	0.00E+00	0.00E+00	1.26E-04
DX1	0.00E+00	0	1-1	-552	-208	694	1	3.02	-299	-724	-380	-2.44E-04	-2.63E-04	-3.41E-05
DY1	0.00E+00	-344	1-2	-280	-393	-826	2	0.00	-2769	502	-739	-2.40E-04	-2.65E-04	1.30E-04
RZ1	1.26E-04	0	2-1	-2769	-739	502	2	7.99	-2508	-16656	-917	-8.37E-04	-2.43E-05	-2.60E-03
DX2	-2.40E-04	0	2-2	-2233	-1104	-21045	3	0.00	-5	-694	483	0.00E+00	0.00E+00	1.26E-04
DY2	2.65E-04	0	3-1	-5	483	-694	3	4.50	14	-624	483	1.47E-04	-3.67E-05	1.89E-06
RZ2	1.30E-04	0	3-2	50	483	-811	4	0.00	420	-524	1438	1.47E-04	-3.67E-05	6.70E-05
DX3	-6.70E-04	0	4-1	420	1438	-524	4	4.60	420	1407	1438	5.95E-04	0.00E+00	1.44E-04
DY3	1.38E-04	0	4-2	420	1438	1407	5	0.00	329	466	2495	1.47E-04	-3.67E-05	6.70E-05
RZ3	1.10E-03	0	5-1	329	2495	466	5	2.62	327	1327	2492	-2.40E-04	-2.65E-04	9.55E-05
DX4	1.47E-04	0	5-2	325	2491	1328	6	0.00	1438	1407	337	5.95E-04	0.00E+00	1.22E-04
DY4	3.67E-05	0	6-1	1438	337	1407	6	6.20	1438	10324	317	-6.70E-04	-1.38E-04	1.05E-03
RZ4	6.70E-05	0	6-2	1438	311	10324	7	0.00	1480	-753	-766	1.47E-04	-3.67E-05	6.70E-05
DX5	5.95E-04	0	7-1	1480	-766	-753	7	7.72	1498	10723	-790	-6.70E-04	-1.38E-04	1.12E-03
DY5	0.00E+00	-757	7-2	1502	-796	10721								
RZ5	1.22E-04	0												
		[

FEA Calculation Results for Roof Plane MP 2 for Freedom Solar, LLC Client Lee Osterhout IDSPL - 2D Frame Analysis of a 2D frame subject to distributed loads, point loads and moments



Scaled 2X Deflected Truss Plot Roof Plane MP 2 for Freedom Solar, LLC Client Lee Osterhout