

iRooFAtm

Instant Roof Framing Analysis

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STRUCTURAL ANALYSIS

for the

ROOFTOP PV SOLAR INSTALLATION

Project: Vonda Nathan Hamilton, 619 Raiford Road, Erwin, NC 28339

Prepared for:



Freedom Solar, LLC

4801 Freidrich Ln, Ste 100 - Austin, TX 78744

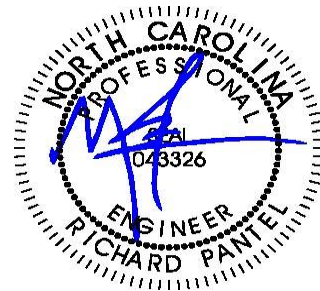
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Project Number: 36.114147, Rev. 0

Report Date: 05/07/2024

Report Prepared by:



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Loading Summary

Exposure and Occupancy Categories	
B	Exposure Category (ASCE 7-16 Table 26.7.3, Page 274)
II	Building Use Occupancy / Risk Category (ASCE 7-16 Table 1.5-1, Page 5)

Wind Loading:			
v	116	mph	Over-ridden per client request. Original data from Municipality provided wind / snow loadings.
qz	20.50	psf	Velocity qz, calculated at height z [ASD]

Snow Loading			
pg	10	psf	Ground Snow Load pg (Over-ridden per client request. Original data from Municipality provided wind / snow loadings.)
Total Snow Load			
ps	10.00	psf	Effective snow load on roof and modules

Module Data			
Mission Solar: MSE395SX9R			
Dimensions	mm	ft	in
Length	1,907	6.26	75.08
Width	1,054	3.46	41.50
Area (m ² , ft ²)	2.0	21.64	
Weight	kg	lb	
Module	22.00	48.50	

Roof Panel (Cladding) Loading Summary		Module Loading Summary			
Support Point Loads		Upward	Upward	Upward	Downward
Roof Zones		1,2e	2n,2r,3e	3r	All
Net load per module	lb	-162	-283	-332	164

Positive values indicate net downward force

Stanchion Fastener Pull-out and Spacing Calculations				
Framing spacing	<i>ft</i>		2.00	
Rails / Module	<i>ea</i>		2	
Max proposed stanchion span	<i>ft</i>		4.00	
# fasteners per stanchion			5	
Screw thread embedment depth	<i>in</i>		0.5	
Safety Factor			1.10	
Pull-out for M5 threaded fasteners	<i>lb/in</i>		103	
Factored max fastener uplift capacity	<i>lb</i>		235	
Fastener details	<i>Material</i>	Stainless	<i>Size</i>	M5
Max stanchion uplift capacity	<i>lb</i>		400	
Max support point uplift capacity	<i>lb</i>		235	

Roof Zones			1,2e	2n,2r,3e	3r
Net lift per module	<i>lb</i>		162	283	332
Min tot screw thread embedment depth req'd	<i>in</i>		0.35	0.60	0.71
Net uplift pressure	7. 0.60D - 0.6W	<i>psf</i>	-6.49	-11.32	-13.25
Allowable lift area / support point		<i>sf</i>	36.24	20.78	17.74
Max rail span per framing spacing		<i>ft</i>	4.00	4.00	4.00

Landscape Modules					
Length along rafter	<i>ft</i>		3.46		
Lift calc'ed max stanchion EW spacing	<i>ft</i>		> 6	> 6	> 6
Max stanchion EW spacing	<i>ft</i>		4.00	4.00	4.00
Maximum module area / support point		<i>sf</i>	6.92	6.92	6.92
Factored lift per support point		<i>lb</i>	-45	-78	-92

Portrait Modules					
Length along rafter	<i>ft</i>		6.26		
Lift calc'ed max stanchion EW spacing	<i>ft</i>		> 6	6.00	4.00
Max stanchion EW spacing	<i>ft</i>		4.00	4.00	4.00
Maximum module area / support point		<i>sf</i>	12.51	12.51	12.51
Factored lift per support point		<i>lb</i>	-81	-142	-166

Plywood Nailing Calculations				
Nail Size	<i>Gauge</i>	<i>Shank Dia</i>	<i>Length</i>	<i>W</i>
8D	10	0.134	2.5	54
10D	9	0.148	3	59
Load Duration Factor - Wind	1.6			
AWC 11.3.1 $W' = W * Cd * Cm * Ct * Ceg * LD$				
8D withdrawal force @ 2" penetration (lb)	138			
10D withdrawal force @ 2.5" penetration (lb)	189			

		1,2e	2n,2r,3e	3r
# 8D's Req'd / stanchion in Landscape	<i>ea</i>	0.32	0.57	0.66
# 10D's Req'd / stanchion in Landscape	<i>ea</i>	0.24	0.41	0.49
# 8D's Req'd / stanchion in Portrait	<i>ea</i>	0.59	1.02	1.20
# 10D's Req'd / stanchion in Portrait	<i>ea</i>	0.43	0.75	0.88

Stanchion support threaded fastener sizes are indicated in the Module Loading Summary table above. Lift forces were determined from GCp and other coefficients contained in the ASCE nomographs

Conclusions

We were asked to review the roof of Vonda Nathan Hamilton, located at 619 Raiford Road, Erwin, NC, by Freedom Solar, LLC, to determine its suitability to support a PV solar system installation.

The referenced building's roof structure was field measured by Freedom Solar, LLC on 04/11/2024. The attached framing analyses reflect the results of those field measurements combined with the PV solar module locations shown on the PV solar roof layout design prepared by Freedom Solar, LLC. Loads are calculated to combine the existing building and environmental loads with the proposed new PV array loads.

The Pegasus PSR-B Rail racking and Roof Tech RT Mini II w 5 M5 screws stanchions were selected for this project by Freedom Solar, LLC. The racking and support stanchions shall be placed as shown on their plans, dated 04/26/2024, and shall be fastened to the roof framing using fastener sizes indicated in this report. Rack support spacing shall be no more than that shown above. Note that support points for alternating rows shall share the same rafter. Intermediate rows shall move the support points laterally to the next rafter. The support rail can be cantilevered up to 1/3 of the maximum span between modules. 1/3 maximum span = 16.00 inches.



Google Location Map

Framing Summary

Based upon the attached calculations, the existing roofs' framing systems are capable of supporting the additional loading for the proposed PV solar system along with the existing building and environmental loads. No supplemental roof framing structural supports are required. Minimum required anchorage fastening is described above.

Fastener notes: 1) Install fasteners with head and where required, washer, flush to material surface (no gap). Do not over-torque.

References and Codes:

- 1) ASCE 7-16 Minimum Design Loads for Buildings and Other Structures
- 2) 2018 IBC
- 3) 2018 NC Building Code
- 4) American Wood Council, NDS 2018, Table 12.2A, 12.3.3A.
- 5) American Wood Council, Wood Structural Design, 1992, Figure 6.

Roof Structural Calculations for PV Solar Installation

Array AR-1

Location: MP 1

Member: Rafter - Total Length 12.4 ft, Unsupported 5.73 ft

Geometric Data			
Θ	deg.	22.02	Angle of roof plane from horizontal, in degrees
ω	deg.	0.00	Angle the solar panel makes with the roof surface
L	ft.	73.00	Length of roof plane, in feet (meters)
W	ft.	12.50	Plan view width of roof plane, in feet (meters)
h	ft.	18.67	Average height of roof above grade, in feet (meters)

Roof Wind Zone Width			
use, a =	3.00	ft	

Wind Velocity Pressure, q_z evaluated at the height z			
q_z =	20.50	psf	$V_{asd} q_z$ = 12.34 psf Basic wind pressure
V=	116		mph

Framing Data	
Wood type	US Spruce
Wood source, moisture content	White 0.12%
# Framing Members / Support	1
Rafter / Truss OC	in 24.00
Member Total Length	ft 12.40

2	# Rafters / Rack Support Width
4.00	Rack Support Spacing (ft)
48	Max. Rack Support Spacing (in)
2	Max # of mod's / Rafter

Member Properties	Member
Name	(1)1.5x3.5
Repetitive Member Factor (Cr)	1.15
Max Shear perp. to grain	psi 530
Max Shear parallel to grain	psi 1,100

* Mem properties based upon field measurements

Rafter

24.00	Collar tie OC spacing, in.
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Module Physical Data			
Weight	kg	lb	psf load
Module	22.00	48.50	2.24
4 Stanchions	2.72	6.0	0.28

Existing Dead Loads	Units	Value	Description
Framing Member	psf	0.50	
Roof Deck & Surface	psf	4.40	0.50 in. Plywood w/ Standard Asphalt Shingles

Rack Support Spacing and Loading			
Across rafters	ft	4.0	
Along rafter slope	ft	6.3	
Area / support point	sf	12.5	
Uphill gap between modules	in	1.0	0.08 ft

Member Total Length	ft	12.40	
Maximum member free span	ft	5.73	Rafter above Knee wall
Rafter segment to calc	ft	5.73	Free span
Deflection Ratio		180	Use max delta 1/x for deflection

* Knee wall height @ 2.50' AFF max height. Adjust to match lowest adjoining roof's collar tie as needed

Eave Overhang Length past Rafter Plate	1.00	ft
Uphill Distance from Eave to Lowest Support	1.50	ft

ASCE 7-16 Method for Calculating Uplift on PV Modules

Notation

L_p = Panel chord length.

p = uplift wind pressure

γ_a = Solar panel pressure equalization factor, defined in Fig. 29.4-8.

γ_E = Array edge factor as defined in Section 29.4.4.

θ = Angle of plane of roof from horizontal, in degrees.

29.4.4 Rooftop Solar Panels Parallel to the Roof Surface on Buildings of All Heights and Roof Slopes.

$\theta \geq 7$ deg TRUE

Min.d1: Exposed	FALSE
Max.d1: Exposed	TRUE
$1.5(L_p) =$	5.19
$\gamma_E =$	1.5
$\gamma_a =$	0.67

Use EXPOSED for uplift calculations

$p = qh(GC_p) (\gamma_E) (\gamma_a) \text{ (lb/ft}^2\text{)} \quad (29.4-7)$

Zones	1,2e	2n,2r,3e	3r
GC _p	-1.48	-2.13	-2.39
p, Windload (psf)	-18.23	-26.28	-29.51

Downward, Zones All Zones
GC_p 0.45

ASCE 7-16 Chapter 2 Combinations of Loads, Table 2.4, Page 8 (in psf)

Zones	1,2e	2n,2r,3e	3r	All Zones
2.2 SYMBOLS AND NOTATION	<i>Module Upward</i>	<i>Module Upward</i>	<i>Module Upward</i>	<i>Downward</i>
D = dead load of PV Module + Stanchion	2.52	2.52	2.52	2.52
S = snow load	10.00	10.00	10.00	10.00
W = wind load	-18.23	-26.28	-29.51	5.58

2.4 Combining Nominal Loads Using Allowable Stress Design (in psf)

2.4.1 Basic Combinations. Loads listed herein shall be considered to act in the following combinations; whichever produces the most unfavorable effect in the building, foundation, or structural member being considered. Effects of one or more loads not acting shall be considered.

Combination Formulae	Upward	Upward	Upward	Downward
Use this loading combination for DOWNWARD for Proposed PV Dead Load				
6. $D + 0.75L - 0.75(0.60W) + 0.75(L_r \text{ or } S \text{ or } R)$	12.52	12.52	12.52	15.03
Module Support point load (lb)	157	157	157	188
Cr Factored Module Support point load (lb)	136	136	136	164

Use this loading combination for UPWARD for Proposed PV Dead Load

7. $0.60D - 0.6W$	-6.49	-11.32	-13.25	7.42
Module Support point load (lb)	-81	-142	-166	93

DOWNWARD

Presume loading directly over member.

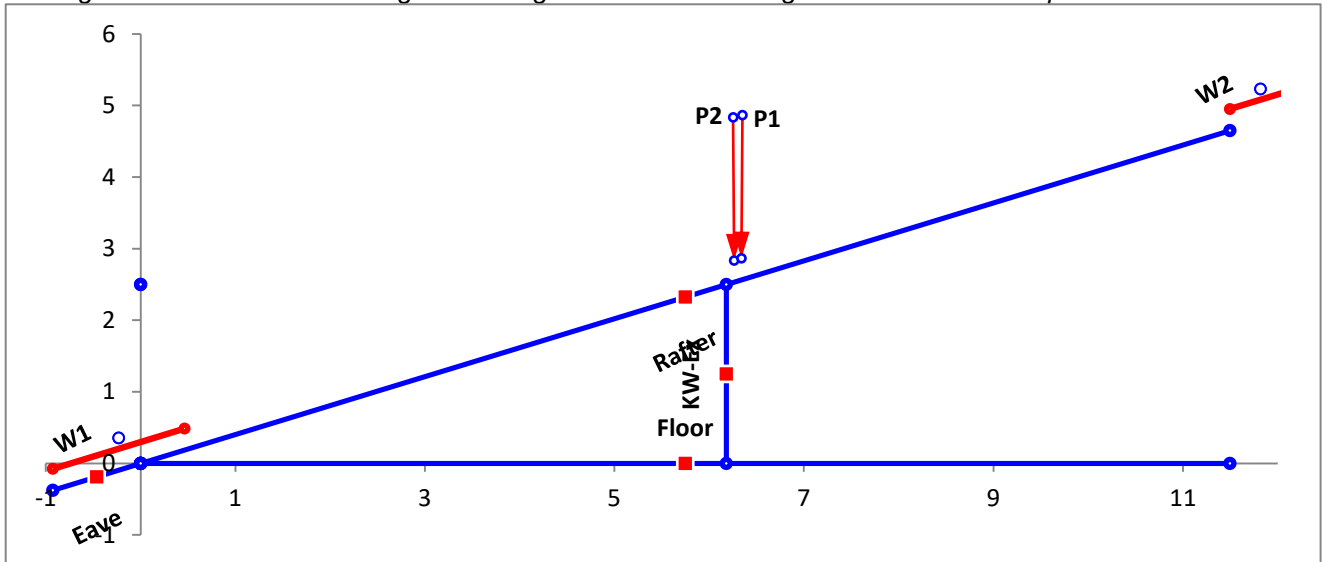
Combined Dead and Wind Pressure Downward Loading					
Rafter above Knee wall					
PV Module Row	Point load loc's from Left support		Module Support Point Load	Comment	Module Orientation
	<i>ft from left</i>		<i>lb</i>		
1	0.50			Support outside of max stressed section	Portrait
1	6.76		164		Portrait
2	6.84		164		Portrait
2	13.10			Support outside of max stressed section	Portrait

Analysis for PV impacted areas

5. Simple Beam - Exposed Roof Snow Load - Above and Below PV				
<i>Parameter</i>	<i>Units</i>	<i>Total</i>	<i>Allowed</i>	<i>Check</i>
Delta @ mid span	<i>in</i>	0.00	0.38	OK
M at mid span	<i>lb-ft</i>	4	1,667	OK

Sum Downward Loading Conditions: PV; Beam DL; Exposed Roof Environmental Load				
<i>Parameter</i>	<i>Units</i>	<i>Total</i>	<i>Allowed</i>	<i>Check</i>
Delta	<i>in</i>	0.04	0.38	OK
Percent Max Delta	<i>%</i>	10%	100%	OK
Moment	<i>lb-ft</i>	940	1,667	OK
fs	<i>psi</i>	3,683	6,533	OK

* Loading includes member self weight & roofing materials. w loading = wind & snow on exposed areas



Framing section with max stress: Rafter above Knee wall

Roof Structural Calculations for PV Solar Installation

Array AR-2

Location: MP 2

Member: Rafter - Total Length 12.49 ft, Unsupported 8.32 ft

Geometric Data			
Θ	deg.	23.00	Angle of roof plane from horizontal, in degrees
ω	deg.	0.00	Angle the solar panel makes with the roof surface
L	ft.	73.00	Length of roof plane, in feet (meters)
W	ft.	12.50	Plan view width of roof plane, in feet (meters)
h	ft.	18.67	Average height of roof above grade, in feet (meters)

Roof Wind Zone Width			
use, a =	3.00	ft	

Wind Velocity Pressure, q_z evaluated at the height z			
$q_z =$	20.50	psf	$V_{asd} q_z =$ 12.34 psf Basic wind pressure
V =	116		mph

Framing Data	
Wood type	US Spruce
Wood source, moisture content	White 0.12%
# Framing Members / Support	1
Rafter / Truss OC	in 24.00
Member Total Length	ft 12.49

2	# Rafters / Rack Support Width
4.00	Rack Support Spacing (ft)
48	Max. Rack Support Spacing (in)
2	Max # of mod's / Rafter

Member Properties	Member
Name	(1)1.5x3.5
Repetitive Member Factor (Cr)	1.15
Max Shear perp. to grain	psi 530
Max Shear parallel to grain	psi 1,100

* Mem properties based upon field measurements

Rafter

24.00	Collar tie OC spacing, in.
-------	----------------------------

Module Physical Data			
Weight	kg	lb	psf load
Module	22.00	48.50	2.24
4 Stanchions	2.72	6.0	0.28

Existing Dead Loads	Units	Value	Description
Framing Member	psf	0.50	
Roof Deck & Surface	psf	4.40	0.50 in. Plywood w/ Standard Asphalt Shingles

Rack Support Spacing and Loading			
Across rafters	ft	4.0	
Along rafter slope	ft	6.3	
Area / support point	sf	12.5	
Uphill gap between modules	in	1.0	0.08 ft

Member Total Length	ft	12.49	
Maximum member free span	ft	8.32	Rafter below Knee wall
Rafter segment to calc	ft	8.32	Free span
Deflection Ratio		180	Use max delta 1/x for deflection

* Knee wall height @ 3.25' AFF max height. Adjust to match lowest adjoining roof's collar tie as needed

Eave Overhang Length past Rafter Plate	1.00	ft
Uphill Distance from Eave to Lowest Support	1.50	ft

ASCE 7-16 Method for Calculating Uplift on PV Modules

Notation

Lp = Panel chord length.

p = uplift wind pressure

ya = Solar panel pressure equalization factor, defined in Fig. 29.4-8.

yE = Array edge factor as defined in Section 29.4.4.

θ = Angle of plane of roof from horizontal, in degrees.

29.4.4 Rooftop Solar Panels Parallel to the Roof Surface on Buildings of All Heights and Roof Slopes.

θ ≥ 7 deg TRUE

Min.d1: Exposed	FALSE
Max.d1: Exposed	TRUE
1.5(Lp) =	5.19
yE =	1.5
ya =	0.67

Use EXPOSED for uplift calculations

p = qh(GCp) (yE) (ya) (lb/ft²) (29.4-7)

Zones	1,2e	2n,2r,3e	3r
GCp	-1.48	-2.13	-2.39
p, Windload (psf)	-18.23	-26.28	-29.51

Downward, Zones All Zones
GCp 0.45

ASCE 7-16 Chapter 2 Combinations of Loads, Table 2.4, Page 8 (in psf)				
Zones	1,2e	2n,2r,3e	3r	All Zones
2.2 SYMBOLS AND NOTATION	<i>Module Upward</i>	<i>Module Upward</i>	<i>Module Upward</i>	<i>Downward</i>
D = dead load of PV Module + Stanchion	2.52	2.52	2.52	2.52
S = snow load	10.00	10.00	10.00	10.00
W = wind load	-18.23	-26.28	-29.51	5.58

2.4 Combining Nominal Loads Using Allowable Stress Design (in psf)				
2.4.1 Basic Combinations. Loads listed herein shall be considered to act in the following combinations; whichever produces the most unfavorable effect in the building, foundation, or structural member being considered. Effects of one or more loads not acting shall be considered.				
<i>Combination Formulae</i>	<i>Upward</i>	<i>Upward</i>	<i>Upward</i>	<i>Downward</i>
Use this loading combination for DOWNWARD for Proposed PV Dead Load				
6. D + 0.75L - 0.75(0.60W) + 0.75(Lr or S or R)	12.52	12.52	12.52	15.03
Module Support point load (lb)	157	157	157	188
Cr Factored Module Support point load (lb)	136	136	136	164

Use this loading combination for UPWARD for Proposed PV Dead Load				
7. 0.60D - 0.6W	-6.49	-11.32	-13.25	7.42
Module Support point load (lb)	-81	-142	-166	93

DOWNWARD

Presume loading directly over member.

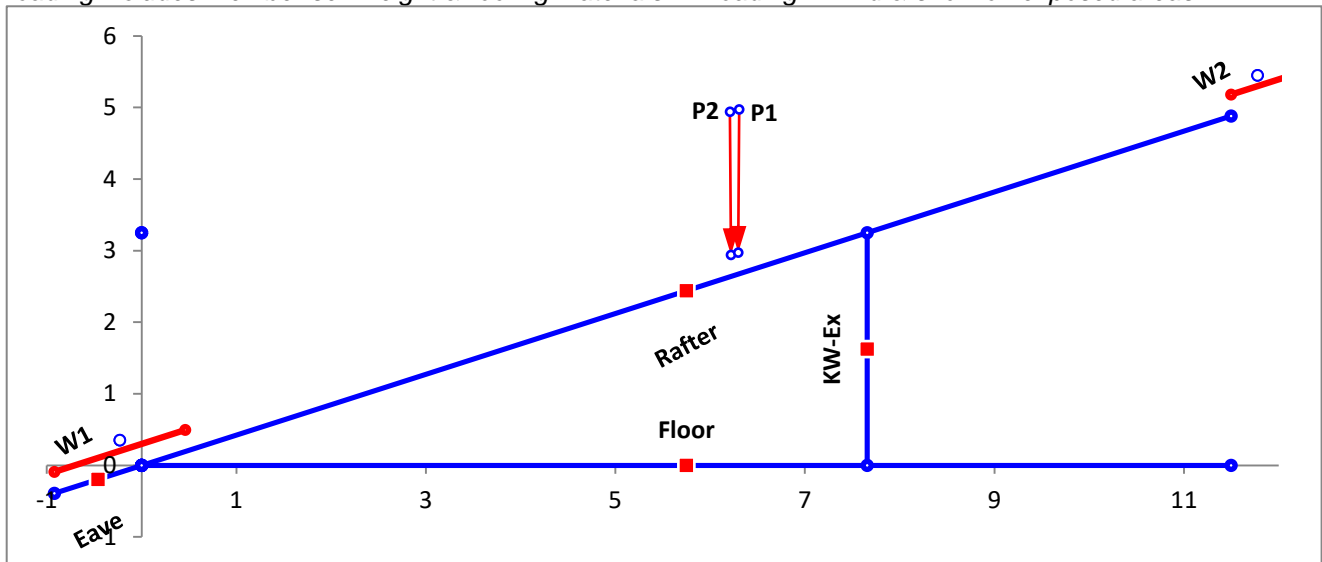
Combined Dead and Wind Pressure Downward Loading					
Rafter below Knee wall					
PV Module Row	Point load loc's from Left support		Module Support Point Load	Comment	Module Orientation
	<i>ft from left</i>		<i>lb</i>		
1	0.50			Support placed on adjoining rafter	Portrait
1	6.76		164		Portrait
2	6.84		164		Portrait
2	13.10			Support outside of max stressed section	Portrait

Analysis for PV impacted areas

5. Simple Beam - Exposed Roof Snow Load - Above and Below PV				
Parameter	Units	Total	Allowed	Check
Delta @ mid span	in	0.01	0.55	OK
M at mid span	lb-ft	3	1,667	OK

Sum Downward Loading Conditions: PV; Beam DL; Exposed Roof Environmental Load				
Parameter	Units	Total	Allowed	Check
Delta	in	0.51	0.55	OK
Percent Max Delta	%	92%	100%	OK
Moment	lb-ft	294	1,667	OK
fs	psi	1,152	6,533	OK

* Loading includes member self weight & roofing materials. w loading = wind & snow on exposed areas



Framing section with max stress: Rafter below Knee wall

Snow Loading Analysis

where:

	Fully Exposed	Exposure category
C_e =	0.9	Exposure Factor, C _e (ASCE 7-16 Table 7.3-1, Page 61)
C_t =	1.0	Thermal Factor, C _t (ASCE 7-16 Table 7.3-2, Page 61)
I_s =	1.0	Snow Importance Factor, I _s (ASCE 7-16 Table 1.5-2, Page 5)
p_g =	10	Ground Snow Load p _g (Over-ridden per client request. Original data from Municipality)

p_f = **0.7C_eC_tI_sP_g** Flat Roof Snow Load, p_f (ASCE 7-16 Table 7.3-1, Page 61)

p_f = **6.3** psf

but where P_f is not less than the following:

Minimum Snow Load p_m (ASCE 7-16 Table 7.3.4, Page 62)

p_m = **10** When P_g <=20 psf, then use P_f = P_g x I_s

p_f = **10** psf. Resultant Snow pressure to be used with Roof slope factor below

p_s = **C_sp_f** Sloped Roof Snow Load p_s (ASCE 7-16 Table 7.4, Page 61)

Roof Type Warm Roofs

Roof slope factor C_s for Warm Roofs, where C_t = 1.0

Roof surface condition = Slippery Roof

C_s = 1.00 Roof Slope Factor, C_s (ASCE 7-16 Table 7.4-1a, Page 62)

Total Snow Load

p_s = 10.00 psf	Roof snow load
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