# RE: Structural Certification for Installation of Residential Solar MEAGHAN NITCHALS:203 E K ST, ERWIN, NC 28339

Attn: To Whom It May Concern

This Letter is for the existing roof framing which supports the new PV modules as well as the attachment of the PV system to existing roof framing. From the field observation report, the roof is made of Metal roofing over roof plywood supported by 2X4 Trusses at 24 inches. The slope of the roof was approximated to be 18 and 30 degrees. The maximum allowable chord span is 8 feet between supports.

After review of the field observation data and based on our structural capacity calculation, the existing roof framing has been determined to be adequate to support the imposed loads without structural upgrades. Contractor shall verify that existing framing is consistent with the described above before install. Should they find any discrepancies, a written approval from SEOR is mandatory before proceeding with install. Capacity calculations were done in accordance with applicable building codes.

#### **Design Criteria**

Code	2018 North Carolina Building Code/IBC 2015					
Risk category		II	Wind Load	(component ar	nd Cladding)	
Roof Dead Load	Dr	10 psf		V(ult)	119 mph	
PV Dead Load	DPV	3 psf		Exposure	С	
<b>Roof Live Load</b>	Lr	20 psf				
<b>Ground Snow</b>	S	10 psf				

If you have any questions on the above, please do not hesitate to call.

Sincerely,



Signed 11/9/2022

# **Structural Letter for PV Installation**

Date: 11/9/2022

Job Address: 203 E K ST

**ERWIN, NC 28339** 

Job Name: **MEAGHAN NITCHALS** 

Job Number: 221109MN

# **Scope of Work**

This Letter is for the existing roof framing which supports the new PV modules as well as the attachment of the PV system to existing roof framing. All PV mounting equipment shall be designed and installed per manufacturer's approved installation specifications.

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# **Engineering Calculations Summary**

<u>Code</u>	2015 International Building Code (ASCE 7-10)		
Risk category		II	
Roof Dead Load	Dr	10 psf	
PV Dead Load	DPV	3 psf	
<b>Roof Live Load</b>	Lr	20 psf	
<b>Ground Snow</b>	S	10 psf	
Wind Load	(component and Claddin	ng)	
	V (Ult)	119 mph	
	Exposure	С	

#### References

2 NDS for Wood Construction

Sincerely,



Signed 11/9/2022

# Wind Load Cont.

Risk Category =	1		ASCE 7-10 Tal	ole 1.5-1
Wind Speed (3s gust), V =	119 mph		ASCE 7-10 Fig	ure 26.5-1A
Roughness =	C A		ASCE 7-10 Sec	c 26.7.2
Exposure =	С		ASCE 7-10 Sec	c 26.7.3
Topographic Factor, K <sub>ZT</sub> =	1.0	00	ASCE 7-10 Sec	26.8.2
Pitch =	18.0	Degrees		
Adjustment Factor, $\lambda =$	1.2	21	ASCE 7-10 Fig	ure 30.5-1
a =	3.60	ft	ASCE 7-10 Fig	ure 30.5-1

Where a: 10% of least horizontal dimension or 0.4h, whichever is smaller, but not less than 4% of least horizontal dimension or 3ft (0.9m)

<u>Uplift (0.6W)</u>	Zone 1 (psf)	Zone 2 (psf)	Zone 3 (psf)	
Pnet30=	-17.8	-25.1	-39.5	Figure 30.5-1
Pnet = 0.6 x λ x KZT x Pnet30)=	12.92	18.21	28.70	Equation 30.5-1
Downpressure (0.6W)	Zone 1 (psf)	Zone 2 (psf)	Zone 3 (psf)	
Pnet30=	9.5	9.5	9.5	Figure 30.5-1
Pnet = 0.6 x λ x KZT x Pnet30)=	6.93	6.93	6.93	Equation 30.5-1

# Rafter Attachments: 0.6D+0.6W (CD=1.6)

### **Connection Check**

	Connection Check			
	Attachement max. spacing=	4	ft	
	S-5 Ultimate Withdrawal Value)=	900	lbs/in	Manufacturer Test
			in	
	Safety Factor	3	in	
	Allowable Capacity=	300		
Zone	Trib Width Area (ft)	Uplift (lbs)	Down (lbs)	
1	4 11.0	122.3	109.2	
2	4 11.0	180.5	109.2	
3	4 11.0	295.9	109.2	
	Max=	295.9	<	300
		CONNECTION	IS OK	

- 1. Pv seismic dead weight is negligible to result in significant seismic uplift, therefore the wind uplift governs
- 2. Embedment is measured from the top of the framing member to the tapered tip of a lag screw. Embedment in sheading or other material does not count.

# **Vertical Load Resisting System Design**

# Roof Framing Trusses

Snow Load Fully Exposed

pg= 10 psf ASCE 7-10 , Section 7.2  $p_f = 7$  psf  $C_e = 0.9$  ASCE 7-10 , Table 7-2  $p_{fmin.} = 10.0$  psf

 $C_{\rm e} = 0.9$  ASCE 7-10 , Table 7-2  ${\bf p_{fmin.}} = {\bf 10.0}$  psf  $C_{\rm t} = 1.1$  ASCE 7-10 , Table 7-3  ${\bf p_s} = {\bf 10}$  psf 16.0 plf

 $I_s = 1.0$  ASCE 7-10 , Table 1.5-1

Max Length, L = 8 ft (Beam maximum Allowable Horizontal Span)

Tributary Width,  $W_T = 24$  in

**Dr = 10** psf 20 plf PvDL = 3 psf 6 plf

Load Case: DL+0.6W

Pnet+  $P_{pv}cos(\theta)+P_{DL}=$  39.9 plf

Max Moment, M<sub>u</sub> = 196 lb-ft Conservatively

Pv max Shear 109.2 lbs Max Shear,  $V_u$ =wL/2+Pv Point Load = 213 lbs

Load Case: DL+0.75(0.6W+S)

0.75(Pnet+Ps)+  $P_{pv}cos(\theta)+P_{DL}=$  48 plf

 $M_{down}$ = 237 lb-ft

Mallowable =  $Sx \times Fb'$  (wind) = 634 lb-ft > 237 lb-ft **OK** 

Load Case: DL+S

Ps+  $P_{pv}$ cos( $\theta$ )+ $P_{DL}$ = 42 plf

 $M_{down}$ = 205 lb-ft

Mallowable =  $Sx \times Fb'$  (wind) = 456 lb-ft > 205 lb-ft **OK** 

Max Shear,  $V_u=wL/2+Pv$  Point Load = 213 lbs

#### **Member Capacity**

DF-L No.2									
2X4	Design Value	C <sub>L</sub>	$C_{F}$	C <sub>i</sub>	$C_r$	K <sub>F</sub>	ф	λ	Adjusted Value
F <sub>b</sub> =	900 psi	1.0	1.5	1.0	1.15	2.54	0.85	0.8	1553 psi
F <sub>v</sub> =	180 psi	N/A	N/A	1.0	N/A	2.88	0.75	0.8	180 psi
E =	1600000 psi	N/A	N/A	1.0	N/A	N/A	N/A	N/A	1600000 psi
E <sub>min</sub> =	580000 psi	N/A	N/A	1.0	N/A	1.76	0.85	N/A	580000 psi

Depth, d = 3.5 in

Width, b = 1.5 in

Cross-Sectonal Area, A =  $5.25 \text{ in}^2$ Moment of Inertia,  $I_{xx} = 5.35938 \text{ in}^4$ 

Section Modulus,  $S_{xx} = 3.0625 \text{ in}^3$ 

Allowable Moment,  $M_{all} = F_b S_{xx} = 396.2 \text{ lb-ft}$  DCR= $M_u / M_{all} = 0.41 < 1$  Satisfactory

Allowable Shear,  $V_{all} = 2/3F_v A = 630.0 \text{ lb}$  DCR= $V_u / V_{all} = 0.34 < 1$  Satisfactory

# **Siesmic Loads Check**

Roof Dead Load	10 psf
% or Roof with Pv	35.1%
Dpv and Racking	3 psf
Averarage Total Dead Load	11.1 psf
Increase in Dead Load	7.0% <b>OK</b>

The increase in seismic Dead weight as a result of the solar system is less than 10% of the existing structure and therefore no further seismic analysis is required.

# **Limits of Scope of Work and Liability**

We have based our structural capacity determination on information in pictures and a drawing set titled PV plans - MEAGHAN NITCHALS. The analysis was according to applicable building codes, professional engineering and design experience, opinions and judgments. The calculations produced for this structure's assessment are only for the proposed solar panel installation referenced in the stamped plan set and were made according to generally recognized structural analysis standards and procedures.