



08-05-2022

Powur PBC

2683 Via De La Valle #321G

Attn.: To Whom It May Concern

re job: Lori Bednash

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The following calculations are for the structural engineering design of the photovoltaic panels and are valid only for the structural info referenced in the stamped plan set. The verification of such info is the responsibility of others.

I certify that the roof structure has sufficient structural capacity for the applied PV loads.

All mounting equipment shall be designed and installed per manufacturer's approved installation specifications.

**Design Criteria:**

Code: 2018 NCSBC, IBC 2018, ASCE 7-16,  
Live Load: 20 psf  
Ult Wind Speed: 119 mph  
Exposure Cat: C  
Ground Snow: 10 psf  
Min Snow Roof: 0 psf

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**Roof Properties:**

Roof 1

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Roof Type = Shingle  
Roof Pitch (deg) = 40.0  
Mean Root Height (ft) = 23.0  
Attachment Trib Width (ft) = 3.25  
Attachment Spacing (ft) = 4.0  
Framing Type = Rafter  
Framing Size = 2x8  
Framing OC Spacing (in.) = 16.0  
Section Thickness, b (in) = 1.5  
Section Depth, d (in) = 7.2  
Section Modulus, S<sub>x</sub> (in<sup>3</sup>) = 13.141  
Moment of Inertia, I<sub>x</sub> (in<sup>4</sup>) = 47.635  
Unsupported Span (ft) = 12.0  
Upper Chord Length (ft) = 16.0  
Deflection Limit D+L (in) = 3.2  
Deflection Limit S or W (in) = 2.133  
Attachments Pattern = Fully Staggered  
Framing Upgrade = No  
Sister Size = NA  
Wood Species = DF  
Wood F<sub>b</sub> (psi) = 900.0  
Wood F<sub>v</sub> (psi) = 180.0  
Wood E (psi) = 1600000.0  
C<sub>D</sub> (wind) = 1.6  
C<sub>d</sub> (snow) = 1.15  
C<sub>LS</sub> = 1.0  
C<sub>M</sub> = C<sub>t</sub> = C<sub>L</sub> = C<sub>i</sub> = 1.0  
C<sub>F</sub> = 1.2  
C<sub>fu</sub> = 1.0  
C<sub>r</sub> = 1.15  
F'<sub>b</sub> wind (psi) = 1987.2  
F'<sub>b</sub> snow (psi) = 1428.3  
F'<sub>v</sub> wind (psi) = 288.0  
F'<sub>v</sub> snow (psi) = 207.0  
M allowable wind (lb-ft) = 2176.09  
M allowable snow (lb-ft) = 1564.06  
V allowable wind (lbs) = 2088.0  
V allowable snow (lbs) = 1500.75  
E' (psi) = 1600000.0



**Load Calculation:**

**Dead Load Calculations:**

Roof 1

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Panels Dead Load (psf) = 3.0  
Roofing Weight (psf) = 3.0  
Decking Weight (psf) = 2.0  
Framing Weight (psf) = 1.869  
Misc. Additional Weight (psf) = 1.0  
Existing Dead Load (psf) = 7.869  
Total Dead Load (psf) = 10.869

**Wind Load Calculations:**

Ultimate Wind Speed (mph) = 119.0  
Directionality Factor,  $k_d$  = 0.85  
Topographic Factor,  $k_{zt}$  = 1.0  
Velocity Press Exp Factor,  $k_z$  = 0.929  
Velocity Pressure,  $q_z$  (psf) = 28.621  
External Pressure Up,  $GCp\_1$  = -1.499  
External Pressure Up,  $GCp\_2$  = -1.769  
External Pressure Up,  $GCp\_3$  = -2.189  
External Pressure Down,  $GCp$  = 0.78  
Design Pressure Up,  $p\_1$  (psf) = -29.602  
Design Pressure Up,  $p\_2$  (psf) = -34.927  
Design Pressure Up,  $p\_3$  (psf) = -43.229  
Design Pressure Down,  $p$  (psf) = 16.0

**Snow Load Calculations:**

Ground Snow Load,  $p_g$  (psf) = 10.0  
Min Flat Snow,  $pf\_min$  (psf) = 0.0  
Sloped Snow,  $ps\_min$  (psf) = 0.0  
Snow Importance Factor,  $I_c$  = 1.0  
Exposure Factor,  $C_e$  = 0.9  
Thermal Factor,  $C_t$  = 1.1  
Flat Roof Snow,  $pf$  (psf) = 6.93  
Slope Factor,  $C_s$  = 1.0  
Sloped Roof Snow,  $ps$  (psf) = 6.93



**Lag Screw Checks:**

Roof 1

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Ref. Withdrawal Value,  $W$  (lb/in) = 266.0

$(C_m = C_t = C_{eg} = 1.0)$  CD = 1.6

Adjusted Withdrawal Value,  $W'$  (lb/in) = 425.6

Lag Penetration,  $p$  (in.) = 2.5

Allowable Withdrawal Force,  $W'p$  (lbs) = 1064.0

Applied Uplift Force (lbs) = -181.778

Uplift DCR = 0.171

Ref. Lateral Value,  $Z$  (lbs) = 266.0

$(C_m = C_t = C_{\Delta} = C_{eg} = 1.0)$  CD = 1.15

Adjusted Lateral Value,  $Z'$  (lbs) = 310.5

Applied Lateral Force (lbs) = 82.977

Angle of Resultant Force,  $\alpha$  (deg) = 1.143

Adjusted Interaction Lateral Value,  $Z'\alpha$  (lbs) = 750.106

Lateral DCR = 0.111



### Roof Framing Checks:

#### Force Checks:

LC1: D+S

Roof 1

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Applied Moment (lb-ft) = 332.0  
Applied Shear (lbs) = 169.0  
Allowable Moment (lb-ft) = 1564.0  
Allowable Shear (lbs) = 1501.0  
Moment DCR = 0.212  
Shear DCR = 0.113

LC2: D+0.6W

Applied Moment (lb-ft) = 382.0  
Applied Shear (lbs) = 194.0  
Allowable Moment (lb-ft) = 2176.0  
Allowable Shear (lbs) = 2088.0  
Moment DCR = 0.176  
Shear DCR = 0.093

LC3: D+0.75(S+0.6W)

Applied Moment (lb-ft) = 434.0  
Applied Shear (lbs) = 221.0  
Allowable Moment (lb-ft) = 2176.0  
Allowable Shear (lbs) = 2088.0  
Moment DCR = 0.2  
Shear DCR = 0.106

LC4: 0.6D+0.6W

Applied Moment (lb-ft) = 301.0  
Applied Shear (lbs) = 153.0  
Allowable Moment (lb-ft) = 2176.0  
Allowable Shear (lbs) = 2088.0  
Moment DCR = 0.138  
Shear DCR = 0.073



**Deflection Checks (Service Level):**

LC1: D+L

Deflection (in.) = 0.144  
Deflection Limit (in.) = 3.2  
Deflection DCR = 0.045

LC2: S

Deflection (in.) = 0.031  
Deflection Limit (in.) = 2.133  
Deflection DCR = 0.014

LC3: W (Down)

Deflection (in.) = 0.03  
Deflection Limit (in.) = 2.133  
Deflection DCR = 0.014

LC4: W (Up)

Deflection (in.) = 0.055  
Deflection Limit (in.) = 2.133  
Deflection DCR = 0.026



**Seismic Check:**

**Existing Weight:**

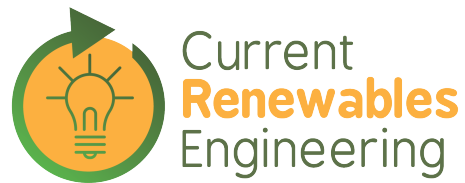
Wall Weight (psf) = 17.0  
Tributary Wall Area (ft<sup>2</sup>) = 3000.0  
Total Wall Weight (lbs) = 51000.0  
Roof Weight (psf) = 7.869  
Roof Area (ft<sup>2</sup>) = 2356.0  
Total Roof Weight (lbs) = 18539.695  
**Total Existing Weight (lbs) = 69539.695**

**Total Additional PV Weight (lbs) = 1608.75**

**Weight Increase:**

$(\text{Existing W} + \text{Additional W}) / (\text{Existing W}) = 1.023$

The increase in weight as a result of the solar system is less than 10% of the existing structure and therefore no further seismic analysis is required.

**Limits of Scope of Work and Liability:**

Existing structure is assumed to have been designed and constructed following appropriate codes at time of erection, and assumed to have appropriate permits. The calculations produced are only for the roof framing supporting the proposed PV installation referenced in the stamped planset and were completed according to generally recognized structural analysis standards and procedures, professional engineering and design experience, opinions and judgements. Existing deficiencies which are unknown or were not observable during time of inspection are not included in this scope of work. All PV modules, racking, and mounting equipment shall be designed and installed per manufacturer's approved installation specifications. The Engineer of Record and the engineering consulting firm assume no responsibility for misuse or improper installation. This analysis is not stamped for water leakage. Framing was determined based on information in provided plans and/or photos, along with engineering judgement. Prior to commencement of work, the contractor shall verify the framing sizes, spacings, and spans noted in the stamped plans, calculations, and cert letter (where applicable) and notify the Engineer of Record of any discrepancies prior to starting construction. Contractor shall also verify that there is no damaged framing that was not addressed in stamped plans, calculations, and cert letter (where applicable) and notify the Engineer of Record of any concerns prior to starting construction.