



March 28, 2022

To: Blue Raven Solar  
1403 North Research Way, Building J  
Orem, UT. 84097

Subject: Certification Letter  
Hines Residence  
423 Mill Bend Dr  
Fuquay-Varina, NC. 27526

To Whom It May Concern,

A jobsite observation of the condition of the existing framing system was performed by an audit team of Blue Raven Solar. All review is based on these observations and the design criteria listed below and only deemed valid if provided information is true and accurate.

On the above referenced project, the roof structural framing has been reviewed for additional loading due to the installation of the solar PV addition to the roof. The structural review only applies to the section of the roof that is directly supporting the solar PV system and its supporting elements. The observed roof framing is described below. If field conditions differ, contractor to notify engineer prior to starting construction.

The roof structure of (MP1) consists of composition shingle on roof plywood that is supported by pre-manufactured trusses that are spaced at @ 24" o.c.. The top chords, sloped at 37 degrees, are 2x4 sections, the bottom chords are 2x4 sections and the web members are 2x4 sections. The truss members are connected by steel gusset plates. The max unsupported projected horizontal top chord span is approximately 6'-0".

The existing roof framing system of (MP1) is judged to be adequate to withstand the loading imposed by the installation of the solar panels. No reinforcement is necessary. Where it is required for standoffs, install vertical 2x6 blocking between truss top chords. Attach block to adjacent trusses with Simpson A34 clips at each end. See attached detail for further specifications.

The spacing of the solar standoffs should be kept at 72" o.c. for landscape and 48" o.c. for portrait orientation, with a staggered pattern to ensure proper distribution of loads.

The scope of this report is strictly limited to an evaluation of the fastener attachment, underlying framing and supporting structure only. The attachment's to the existing structure are required to be in a staggered pattern to ensure proper distribution of loading. All panels, racking and hardware shall be installed per manufacturer specifications and within specified design limitations. All waterproofing shall be provided by the manufacturer.

Note: Seismic check is not required since  $S_s < .4g$  and Seismic Design Category (SDC) < B

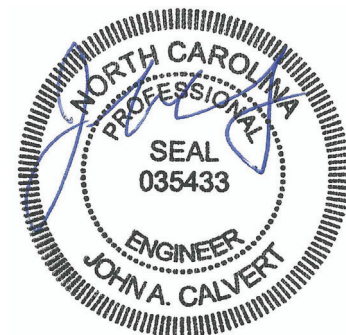
Design Criteria:

- Applicable Codes = 2018 North Carolina State Building Code (NCSBC), ASCE 7-10
- Roof Dead Load = 7 psf (MP1)
- Roof Live Load = 20 psf
- Wind Speed = 115 mph (Vult), Exposure C, Risk Category II
- Ground Snow Load = 15 psf - Roof Snow Load = 10.5 psf
- Attachment: 1 - 5/16 dia. lag screw with 2.5 inch min. embedment depth, at spacing shown above.

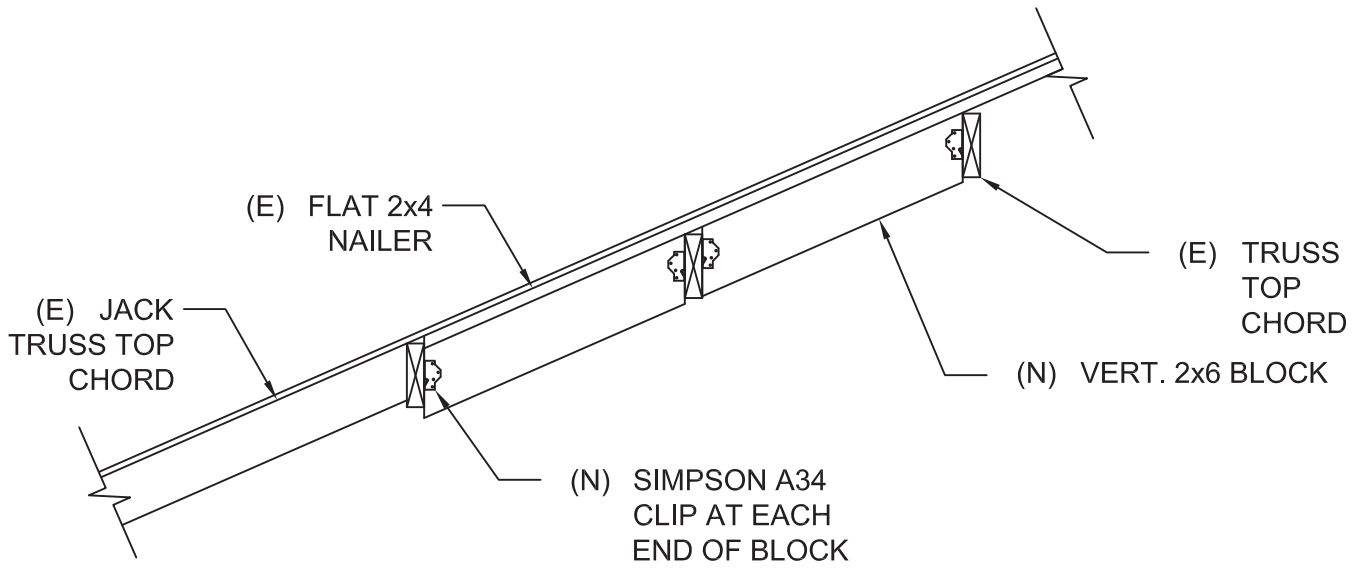
Please contact me with any further questions or concerns regarding this project.

Sincerely,

John Calvert, P.E.  
Project Engineer



John A. Calvert  
Digitally signed by John A. Calvert  
Date: 2022.03.28 10:02:56 -06'00'



W1

# TRUSS BLOCK INSTALL - ELEV.



PROJECT NAME: Blocking Install		Scale: N.T.S.	
		Date: 9/20/16	
		Project Number: Solar PV	
	Project Description: Blocking for standoff attachment	Drawn By: JAC	Drawing Name: <b>BLK1</b>
		Revisions:	
		A	
		B	



### Gravity Loading

Roof Snow Load Calculations		
$p_g$ = Ground Snow Load =	15 psf	
$p_f = 0.7 C_e C_t I p_g$		(ASCE7 - Eq 7-1)
$C_e$ = Exposure Factor =	1	(ASCE7 - Table 7-2)
$C_t$ = Thermal Factor =	1	(ASCE7 - Table 7-3)
$I$ = Importance Factor =	1	
$p_f$ = Flat Roof Snow Load =	10.5 psf	
$p_s = C_s p_f$		(ASCE7 - Eq 7-2)
$C_s$ = Slope Factor =	1	
<b><math>p_s</math> = Sloped Roof Snow Load =</b>	<b>10.5 psf</b>	

PV Dead Load = 3 psf (Per Blue Raven Solar)	
DL Adjusted to 37 Degree Slope	3.76 psf
PV System Weight	
Weight of PV System (Per Blue Raven Solar)	3.0 psf
X Standoff Spacing =	4.00 ft
Y Standoff Spacing =	6.08 ft
Standoff Tributary Area =	24.33 sft
<b>Point Loads of Standoffs</b>	<b>73 lb</b>
Note: PV standoffs are staggered to ensure proper distribution of loading	

Roof Live Load = 20 psf	
Note: Roof live load is removed in area's covered by PV array.	

Roof Dead Load (MP1)		
Composition Shingle	4.00	
Roof Plywood	2.00	
2x4 Top Chords @ 24"o.c.	0.73	
Vaulted Ceiling	0.00	(Ceiling Not Vaulted)
Miscellaneous	0.27	
<b>Total Roof DL (MP1)</b>	<b>7.0 psf</b>	
DL Adjusted to 37 Degree Slope	8.8 psf	



**Wind Calculations**

**Per ASCE 7-10 Components and Cladding**

Input Variables	
Wind Speed	115 mph
Exposure Category	C
Roof Shape	Hip/Gable
Roof Slope	37 degrees
Mean Roof Height	20 ft
Effective Wind Area	21.3 ft

Design Wind Pressure Calculations	
<b>Wind Pressure P = qh * G * Cn</b>	
qh = 0.00256 * Kz * Kzt * Kd * V^2	(Eq. 30.3-1)
Kz (Exposure Coefficient) = 0.9	(Table 30.3-1)
Kzt (topographic factor) = 1	(Fig. 26.8-1)
Kd (Wind Directionality Factor) = 0.85	(Table 26.6-1)
V (Design Wind Speed) = 115 mph	(Fig. 26.5-1A)
Risk Category = II	(Table 1.5-1)
qh = 25.90	
0.6 * qh = 15.54	

Standoff Uplift Calculations-Portrait					
	Zone 1	Zone 2	Zone 3	Positive	
GCp =	-0.94	-1.15	-1.15	0.86	(Fig. 30.4-1)
Uplift Pressure =	-14.55 psf	-17.80 psf	-17.80 psf	22.4 psf	
X Standoff Spacing =	4.00	4.00	2.67		
Y Standoff Spacing =	6.08	3.041666667	3.041666667		
Tributary Area =	24.33	12.17	8.11		
Dead Load on Attachment =	73.00	36.50	24.33		
<b>Footing Uplift (0.6D+0.6W) =</b>	<b>-310 lb</b>	<b>-195 lb</b>	<b>-130 lb</b>		

Standoff Uplift Calculations-Landscape					
	Zone 1	Zone 2	Zone 3	Positive	
GCp =	-0.94	-1.15	-1.15	0.86	(Fig. 30.4-1)
Uplift Pressure =	-14.55 psf	-17.80 psf	-17.80 psf	10.5 psf	
X Standoff Spacing =	6.00	6.00	4.00		
Y Standoff Spacing =	3.50	1.75	1.75		
Tributary Area =	21.00	10.50	7.00		
Dead Load on Attachment =	63.00	31.50	21.00		
<b>Footing Uplift (0.6D+0.6W) =</b>	<b>-268 lb</b>	<b>-168 lb</b>	<b>-112 lb</b>		

Standoff Uplift Check	
Maximum Design Uplift =	-310 lb
Standoff Uplift Capacity =	450 lb
450 lb capacity > 310 lb demand	Therefore, OK

Fastener Capacity Check	
Fastener =	1 - 5/16" dia. lag
Number of Fasteners =	1
Embedment Depth =	2.5
Pullout Capacity Per Inch =	250 lb
Fastener Capacity =	625 lb
w/ F.S. of 1.5 & DOL of 1.6 =	667 lb
667.2 lb capacity > 310 lb demand	Therefore, OK



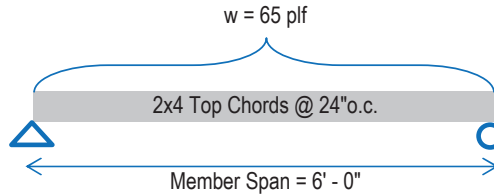
**Framing Check**

(MP1)

**PASS**

Dead Load        8.8 psf  
 PV Load         3.8 psf  
 Live Load        20.0 psf

Governing Load Combo = DL + LL  
**Total Load        32.5 psf**



Member Properties				
Member Size	S (in <sup>3</sup> )	I (in <sup>4</sup> )	Lumber Sp/Gr	Member Spacing
2x4	3.06	5.36	DF#2	@ 24"o.c.

Check Bending Stress								
Fb (psi) =	fb	x	Cd	x	Cf	x	Cr	(NDS Table 4.3.1)
	900	x	1.25	x	1.5	x	1.15	
Allowed Bending Stress = 1940.6 psi								

Maximum Moment = (wL<sup>2</sup>) / 8  
 = 292.6922 ft#  
 = 3512.307 in#  
 Actual Bending Stress = (Maximum Moment) / S  
 = 1146.9 psi

**Allowed > Actual -- 59.2% Stressed -- Therefore, OK**

Check Deflection		
Allowed Deflection (Total Load) =	L/180	(E = 1600000 psi Per NDS)
	= 0.4 in	
Deflection Criteria Based on =	Continuous Span	
Actual Deflection (Total Load) =	(w*L <sup>4</sup> ) / (185*E*I)	
	= 0.092 in	
	= L/783 > L/180	<b>Therefore OK</b>
Allowed Deflection (Live Load) =	L/240	
	0.3 in	
Actual Deflection (Live Load) =	(w*L <sup>4</sup> ) / (185*E*I)	
	0.057 in	
	L/1264 > L/240	<b>Therefore OK</b>

Check Shear		
Member Area = 5.3 in <sup>2</sup>	Fv (psi) = 180 psi	(NDS Table 4A)
Allowed Shear = Fv * A = 945 lb	Max Shear (V) = w * L / 2 =	195 lb

**Allowed > Actual -- 20.7% Stressed -- Therefore, OK**