

January 11, 2022

BES Project Number: 5436 Roneil Swaby

Power Home Solar, LLC 919 N Main St. Mooresville, NC 28115

Project Location: Roneil Swaby: 402 New Castle Ln., Spring Lake, NC 28390 Solar Array Installation

To Whom It May Concern:

Per your request, BES has reviewed the existing structure at the above referenced location. The purpose of this review was to determine the adequacy of the existing structure to support the proposed installation of solar panels on the roof as shown on the attached panel layout plan.

Based upon our review, we certify that existing roof structure will adequately support with the following: Racking and attachment mounting connection: (1) 5/16" lag screw w/min. 2.5" embedment into framing at max 48" o/c along rails (2) rails per row of panels, evenly spaced; panel length perpendicular to the rails not to exceed 67 in. Solar module mounting hardware design is by the manufacturer.

Limitations: Installation of the solar panels must be performed in accordance with manufacturer recommendations. All work performed must be in accordance with accepted industry-wide methods and applicable safety standards. The contractor must notify BES should any damage, deterioration or discrepancies between the as-built condition of the structure and the condition described in this letter be found. Connections to existing roof framing must be staggered, except at array ends, so as to not overload any existing structural member. The design of the solar panel racking (mounts, rails, etc.) is the responsibility of the manufacturer. Waterproofing around the roof penetrations is the responsibility of others. BES assumes no responsibility for improper installation of the solar array. Existing structure meets or exceeds standard building practices with current building code with assumed single layer asphalt shingles.

Sincerely,



Jermey Bowers M.E., P.E. *Principal Engineer*

Bowers Engineering Services 121 S. Main ST Auburn, IN (260) 333-0900

Structural Analysis

Location

402 New Castle Ln Spring Lake, NC 28390

Roof Mount Solar

1/11/2022



Project: 5436

Rev:

-

Page 1 of 5

BES			Date:	1/11/2022	Connections
121 South Main ST					
Auburn, IN					
Cust. Name:	Bowers Engineering Serv	ices	Subject:	Roof Mount	
Job Number:	5436	0	riginatoi	0	Checker:
	<u>STRUCTUR</u>	<u>4L SUMM</u>	ARY		
<u>CODE SPEC</u>	W	/IND			
IBC 2015		Speed.	119	МРН	
ASCE 7-10		Evn :	C	1011 11	
TISCE / TO		LAP	C		
Risk Cat:	II				
Wind Load - uplift					
			Max lb		
Zone 1	-28.71 psf		-192.93	lb	
Zone 2	-34.50 psf		-231.87	lb	
Zone 3	-34.50 psf		-231.87	lb	
Max trib	11.20 ft2				
Max loading at connection					
Negitive	-231.87 lb/fastener				
Connection (Pull Out)					
Lag screw	5/16 in				
Cd	1.60 Table 2.3.2				
embedment	2.5 in				
Nominal CanacityPrving	205.00 lbs G=0.42				
Max capacity (lbs)	533.00	>	231.87		ОК
Note:					
* Lag screws to be diameter	5/16x2.5inches long.				

* All fasteners need to be placed at roof rafters.

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BES 121 South Main ST Auburn, IN			V	WIND LOADING Per ASCE 7-10
Cust Name:	Bowers Engineering Services	Subject:	Roof Mount	
Job Number:	5436	Originator:	0	Checker:

Input Data:

Wind Speed, V =	119	mph (Wind Map, Figure 26.5-1A-C)
Bldg. Classification =	II	(Table 1-1 Occupancy Category)
Exposure Category =	С	(Sect. 26.7)
Ridge Height, hr =	28.75	ft. (hr >= he)
Eave Height, he =	20.00	ft. (he <= hr)
Building Width =	30.00	ft. (Normal to Building Ridge)
Building Length =	36.00	ft. (Parallel to Building Ridge)
Roof Type =	Gable	(Gable or Monoslope)
Topo. Factor, Kzt =	1.00	(Sect. 26.8 & Figure 26.8-1)
Direct. Factor, Kd =	0.85	(Table 26.6)
Enclosed? (Y/N)	Y	(Sect. 28.6-1 & Figure 26.11-1)
Hurricane Region?	N	
Component Name =	Decking	(Purlin, Joist, Decking, or Fastener)
Effective Area, Ae =	11.1	ft.^2 (Area Tributary to C&C)
Overhangs? (Y/N)	N	(if used, overhangs on all sides)





Resulting Parameters and Coefficients:

Roof Angle, $\theta = 30.26$ deg. Mean Roof Ht., h = 24.38 ft. (h = (hr+he)/2, for roof angle >10 deg.)

Roof External Pressure Coefficients, GCp:

GCp Zone 1-3 Pos. = (Fig. 30.4-2A, 30.4-2B, and 30.4-2C) 0.90 GCp Zone 1 Neg. = -0.99 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C) GCp Zone 2 Neg. = -1.19 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C) (Fig. 30.4-2A, 30.4-2B, and 30.4-2C) GCp Zone 3 Neg. = -1.19 Positive & Negative Internal Pressure Coefficients, GCpi (Figure 26.11-1): +GCpi Coef. = 0.00 (positive internal pressure) -GCpi Coef. = 0.00 (negative internal pressure) If $z \le 15$ then: $Kz = \overline{2.01^*(15/zg)}^{(2/\alpha)}$, If z > 15 then: $Kz = 2.01^*(z/zg)^{(2/\alpha)}$ (Table 30.3-1) α= 9.50 (Table 26.9-1) zg = 900 (Table 26.9-1) 0.94 Kh = (Kh = Kz evaluated at z = h)

Velocity Pressure: qz = 0.00256^{Kz} Kzt*Kd*V² (Sect. 30.3.2, Eq. 30.3-1) qh = 28.97 psf qh = 0.00256^{Kh} Kzt*Kd*V² (qz evaluated at z = h)

Design Net External Wind Pressures (Sect. 30.4 & 30.6): For h <= 60 ft.: p = qh*((GCp) - (+/-GCpi)) (psf) For h > 60 ft.: p = q*(GCp) - qi*(+/-GCpi) (psf) where: q = qh for roof qi = qh for roof (conservatively assumed per Sect. 30.6)

PAGE 3 of 5

Wind Load Tabulation for Roof Components & Cladding							
Component	Z	Kh	qh	p:	= Net Design	Pressures (osf)
	(ft.)		(psf)	Zone 1,2,3 (+)	Zone 1 (-)	Zone 2 (-)	Zone 3 (-)
Decking	0	0.94	28.97	25.94	-28.71	-34.50	-34.50
	15.00	0.94	28.97	25.94	-28.71	-34.50	-34.50
	20.00	0.94	28.97	25.94	-28.71	-34.50	-34.50
	25.00	0.94	28.97	25.94	-28.71	-34.50	-34.50
For z = he:	20.00	0.94	28.97	25.94	-28.71	-34.50	-34.50
For $z = h$:	24.38	0.94	28.97	25.94	-28.71	-34.50	-34.50

ft.

Notes: 1. (+) and (-) signs signify wind pressures acting toward & away from respective surfaces.

- 2. Width of Zone 2 (edge), 'a' = 3.00
- 3. Width of Zone 3 (corner), 'a' = 3.00 ft.

4. For monoslope roofs with $\theta \le 3$ degrees, use Fig. 30.4-2A for 'GCp' values with 'qh'.

5. For buildings with h > 60' and θ > 10 degrees, use Fig. 30.6-1 for 'GCpi' values with 'qh'.

- 6. For all buildings with overhangs, use Fig. 30.4-2B for 'GCp' values per Sect. 30.10.
- 7. If a parapet >= 3' in height is provided around perimeter of roof with $\theta \leq 10$ degrees, Zone 3 shall be treated as Zone 2.
- 8. Per Code Section 30.2.2, the minimum wind load for C&C shall not be less than 16 psf.
- 9. References : a. ASCE 7-02, "Minimum Design Loads for Buildings and Other Structures".
 - b. "Guide to the Use of the Wind Load Provisions of ASCE 7-02" by: Kishor C. Mehta and James M. Delahay (2004).

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Roof Components and Cladding:







 $\frac{\text{Roof Zones for Buildings with h > 60 ft.}}{\text{(for Gable Roofs <= 10° and Monoslope Roofs <= 3°)}}$

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Frame Design				General Inf	0	
Cust. Name:	Bowers Engineering Se	rvices	Subject:	Roof Mount		
Job Number:	5436		Originator:		Check	er:
Date:	1/11/22					
Address	402 New Castle Ln	Rev:	-			
City, State:	Spring Lake, NC 28390					

Roof Rafter

		<u>R</u>	oof Loads		
2x4	SYP #1		Dead Load=	8.00	psf
			Live Load=	20	psf
2	ft		Snow Load=	10	psf
8.5	ft				
(1.00	10	Load	Combination	20.5	C
61.00 550.91	pii lb_ft	D	+0./5L+0./58	30.5	psi
550.91	10-11		FI=	8 6E+06	ib-in
Roof Materials			$S_{X} =$	3.0625	10 111
2	psf		C _M =	1.0	
3	psf		Cr=	1.2	
0.50	psf		$C_D =$	1.15	
2.50	psf		$C_{F} =$	1.3	
-frame wood roof*			$C_L =$	1.0	
M . 10			Fb=	1500	psi
$b = \frac{M * 12}{2}$					
Sx		fb=	2158.65	psi	
* Cr * Cf * Cm * Cl		F'b=	2578.88	psi	OK
$\Delta L=$		0.55 in			
$\Delta S =$		0.27 in			
$\Delta D+L=$		0.77 in			
				<u>l/120</u>	
$\Delta_{\text{allow in}} =$	0.77	/ <		0.85	OK
				<u>l/180</u>	
$\Delta_{\text{allow in}} =$	0.55	5 <		0.57	OK
2x4	a		2	o/c	OK
	$2x4$ 2 8.5 61.00 550.91 $\frac{Roof Materials}{2}$ 2 3 0.50 2.50 -frame wood roof* $\phi = \frac{M * 12}{Sx}$ $* Cr * Cf * Cm * Cl$ $\Delta L=$ $\Delta S=$ $\Delta D+L=$ $\Delta allow in=$ $\Delta_{allow in}=$ $\Delta_{allow in}=$	2x4SYP #12ft8.5ft61.00plf550.91lb-ftBoof Materials2psf3psf0.50psf2.50psf-frame wood roof*psf $\phi = \frac{M * 12}{Sx}$ $x Cr * Cf * Cm * Cl$ $\Delta L = \Delta S = \Delta D + L = \Delta allow in = 0.77$ $\Delta allow in = 0.55$	$2x4$ $SYP #1$ $2x4$ $SYP #1$ $\frac{2}{8.5}$ ft $\frac{1000}{550.91}$ $\frac{91f}{1b-ft}$ $\frac{100}{1b-ft}$ $\frac{100}{550.91}$ $\frac{100}{1b-ft}$ $\frac{100}{100}$ $\frac{100}{550.91}$ $\frac{2}{550.91}$ $\frac{100}{100}$ $\frac{100}{550.91}$ $\frac{100}{100}$ $\frac{100}{550.91}$ $\frac{100}{100}$ $$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

Assume rafters are fully braced

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121 South Main ST					
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Job Number:	5436	0	riginator	0	Checker:
	<u>STRUCTUR</u>	<u>AL SUMM</u>	ARY		
<u>CODE SPEC</u>	11				
IDC 2015	W	(IND	110 1	(5)1	
IBC 2015		Speed:	119 N	MPH	
ASCE /-10		Exp.:	С		
Risk Cat:	II				
Wind Load - uplift					
Ĩ			Max lb		
Zone 1	-28.49 psf		-191.45 1	b	
Zone 2	-34.24 psf		-230.1 1	Ь	
Zone 3	-34.24 psf		-230.1 1	b	
Max trib	11.20 ft2				
Max loading at connection					
Negitive	-230.10 lb/fastener				
Connection (Pull Out)					
Lag screw	5/16 in				
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Topo. Factor, Kzt =	1.00	(Sect. 26.8 & Figure 26.8-1)
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Enclosed? (Y/N)	Y	(Sect. 28.6-1 & Figure 26.11-1)
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Component Name =	Decking	(Purlin, Joist, Decking, or Fastener)
Effective Area, Ae =	11.1	ft.^2 (Area Tributary to C&C)
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Resulting Parameters and Coefficients:

Roof Angle, $\theta = 30.26$ deg. Mean Roof Ht., h = 23.50 ft. (h = (hr+he)/2, for roof angle >10 deg.)

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Velocity Pressure: qz = 0.00256^{Kz} Kz^{*}Kd^{*}V² (Sect. 30.3.2, Eq. 30.3-1) qh = 28.75 psf qh = 0.00256^{Kh} Kzt^{*}Kd^{*}V² (qz evaluated at z = h)

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	15.00	0.93	28.75	25.75	-28.49	-34.24	-34.24	
	20.00	0.93	28.75	25.75	-28.49	-34.24	-34.24	
	25.00	0.93	28.75	25.75	-28.49	-34.24	-34.24	
For z = he:	20.00	0.93	28.75	25.75	-28.49	-34.24	-34.24	
For $z = h$:	23.50	0.93	28.75	25.75	-28.49	-34.24	-34.24	

ft.

Notes: 1. (+) and (-) signs signify wind pressures acting toward & away from respective surfaces.

- 2. Width of Zone 2 (edge), 'a' = 3.00
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Frame Design				General Inf	0	
Cust. Name:	Bowers Engineering Se	rvices	Subject:	Roof Mount		
Job Number:	5436		Originator:		Check	er:
Date:	1/11/22					
Address	402 New Castle Ln	Rev:	-			
City, State:	Spring Lake, NC 28390					

Roof Rafter

		<u>R</u>	oof Loads		
2x4	SYP #1		Dead Load=	8.00	psf
			Live Load=	20	psf
2	ft		Snow Load=	10	psf
8.5	ft				
(1.00	10	Load	Combination	20.5	C
61.00 550.91	pii lb_ft	D	+0./5L+0./58	30.5	psi
550.91	10-11		FI=	8 6E+06	ib-in
Roof Materials			$S_X =$	3.0625	10 111
2	psf		C _M =	1.0	
3	psf		Cr=	1.2	
0.50	psf		$C_D =$	1.15	
2.50	psf		$C_{F} =$	1.3	
-frame wood roof*			$C_L =$	1.0	
M . 10			Fb=	1500	psi
$b = \frac{M * 12}{2}$					
Sx		fb=	2158.65	psi	
* Cr * Cf * Cm * Cl		F'b=	2578.88	psi	OK
$\Delta L=$		0.55 in			
$\Delta S =$		0.27 in			
$\Delta D+L=$		0.77 in			
				<u>l/120</u>	
$\Delta_{\text{allow in}} =$	0.77	/ <		0.85	OK
				<u>l/180</u>	
$\Delta_{\text{allow in}} =$	0.55	5 <		0.57	OK
2x4	a		2	o/c	OK
	$2x4$ 2 8.5 61.00 550.91 $\frac{Roof Materials}{2}$ 2 3 0.50 2.50 -frame wood roof* $\phi = \frac{M * 12}{Sx}$ $* Cr * Cf * Cm * Cl$ $\Delta L=$ $\Delta S=$ $\Delta D+L=$ $\Delta allow in=$ $\Delta_{allow in}=$ $\Delta_{allow in}=$	2x4SYP #12ft8.5ft61.00plf550.91lb-ftBoof Materials2psf3psf0.50psf2.50psf-frame wood roof*psf $\phi = \frac{M * 12}{Sx}$ $x Cr * Cf * Cm * Cl$ $\Delta L = \Delta S = \Delta D + L = \Delta allow in = 0.77$ $\Delta allow in = 0.55$	$2x4$ $SYP #1$ $2x4$ $SYP #1$ $\frac{2}{8.5}$ ft $\frac{1000}{550.91}$ $\frac{91f}{1b-ft}$ $\frac{100}{1b-ft}$ $\frac{100}{550.91}$ $\frac{100}{1b-ft}$ $\frac{100}{100}$ $\frac{100}{550.91}$ $\frac{2}{550.91}$ $\frac{100}{100}$ $\frac{100}{550.91}$ $\frac{100}{100}$ $\frac{100}{550.91}$ $\frac{100}{100}$ $$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

Assume rafters are fully braced