

January 10, 2022

BES Project Number: 5416 Jose Padellajimenez

Power Home Solar, LLC 919 N Main St. Mooresville, NC 28115

> Project Location: Jose Padellajimenez: 14 Gloucester Ct., Cameron, NC 28326 Solar Array Installation

To Whom It May Concern:

Per your request, BES has reviewed the existing structure at the above referenced location. The purpose of this review was to determine the adequacy of the existing structure to support the proposed installation of solar panels on the roof as shown on the attached panel layout plan.

Based upon our review, we certify that existing roof structure will adequately support with the following: Racking and attachment mounting connection: (1) 5/16" lag screw w/ min. 2.5" embedment into framing at max 48" o/c along rails (2) rails per row of panels, evenly spaced; panel length perpendicular to the rails not to exceed 67 in. Solar module mounting hardware design is by the manufacturer.

Limitations: Installation of the solar panels must be performed in accordance with manufacturer recommendations. All work performed must be in accordance with accepted industry-wide methods and applicable safety standards. The contractor must notify BES should any damage, deterioration or discrepancies between the as-built condition of the structure and the condition described in this letter be found. Connections to existing roof framing must be staggered, except at array ends, so as to not overload any existing structural member. The design of the solar panel racking (mounts, rails, etc.) is the responsibility of the manufacturer. Waterproofing around the roof penetrations is the responsibility of others. BES assumes no responsibility for improper installation of the solar array. Existing structure meets or exceeds standard building practices with current building code with assumed single layer asphalt shingles.

Sincerely,



Jermey Bowers M.E., P.E. *Principal Engineer*

Bowers Engineering Services 121 S. Main ST Auburn, IN (260) 333-0900

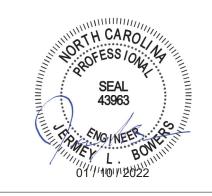
Structural Analysis

Location

14 Gloucester Ct Cameron, NC 28326

Roof Mount Solar

1/10/2022



Project: 5416 Rev:

BES		Date:	1/10/2022	Connections
121 South Main ST				
Auburn, IN				
Cust. Name:	Bowers Engineering Services	Subject: Ro	oof Mount	
Job Number:	5416	Originator	0	Checker:
	<u>STRUCTURAL SU</u>	<u> </u>		
CODE SPEC	STRUCTURAL SC	OIVIIVIAN I		
<u>CODE SPEC</u>	WIND	<u>MMAKT</u>		

Exp.:

 \mathbf{C}

Wind Load - uplift

ASCE 7-10

Risk Cat:

Max lb

Zone 1 -27.82 psf -186.95 lb

Zone 2 -33.43 psf -224.68 lb

Zone 3 -33.43 psf -224.68 lb

Max trib 11.20 ft2

Max loading at connection

Negitive -224.68 lb/fastener

Connection (Pull Out)

Lag screw 5/16 in

 \parallel

Cd 1.60 Table 2.3.2

embedment 2.5 in

Nominal CapacityPrying 205.00 lbs G=0.42

Max capacity (lbs) 533.00 > 224.68 **OK**

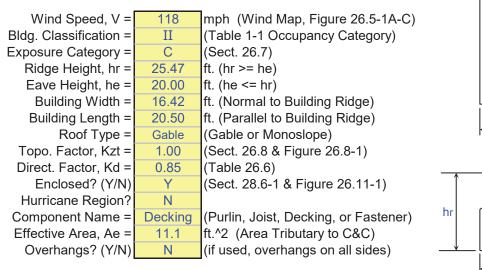
Note:

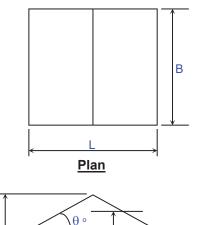
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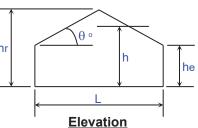
^{*} All fasteners need to be placed at roof rafters.

BES			/	WIND LOAD	ING
121 South Main ST				Per ASCE 7-	-10
Auburn, IN					
Cust Name:	Bowers Engineering Services	Subject:	Roof Mount		
Job Number:	5416	Originator:	0	Checker:	

Input Data:







Resulting Parameters and Coefficients:

```
Roof Angle, \theta = 33.69 deg.
Mean Roof Ht., h = 22.74 ft. (h = (hr+he)/2, for roof angle > 10 deg.)
```

Roof External Pressure Coefficients, GCp:

```
GCp Zone 1-3 Pos. = 0.90 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
GCp Zone 1 Neg. = -0.99 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
GCp Zone 2 Neg. = -1.19 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
GCp Zone 3 Neg. = -1.19 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
Costitute 8 Negative Internal Proseure Coefficients (GCp) (Figure 26.11.1)
```

Positive & Negative Internal Pressure Coefficients, GCpi (Figure 26.11-1):

+GCpi Coef. = 0.00 (positive internal pressure)
-GCpi Coef. = 0.00 (negative internal pressure)

If $z \le 15$ then: $Kz = 2.01*(15/zg)^{(2/\alpha)}$, If z > 15 then: $Kz = 2.01*(z/zg)^{(2/\alpha)}$ (Table 30.3-1) $\alpha = 9.50$ (Table 26.9-1)

zg = 900 (Table 26.9-1) Kh = 0.93 (Kh = Kz evaluated at z = h)

Velocity Pressure: $qz = 0.00256*Kz*Kzt*Kd*V^2$ (Sect. 30.3.2, Eq. 30.3-1) qh = 28.07 psf $qh = 0.00256*Kh*Kzt*Kd*V^2$ (qz evaluated at z = h)

Design Net External Wind Pressures (Sect. 30.4 & 30.6):

For $h \le 60 \text{ ft.: } p = qh*((GCp) - (+/-GCpi)) \text{ (psf)}$

For h > 60 ft.: $p = q^*(GCp) - qi^*(+/-GCpi)$ (psf)

where: q = qh for roof

qi = qh for roof (conservatively assumed per Sect. 30.6)

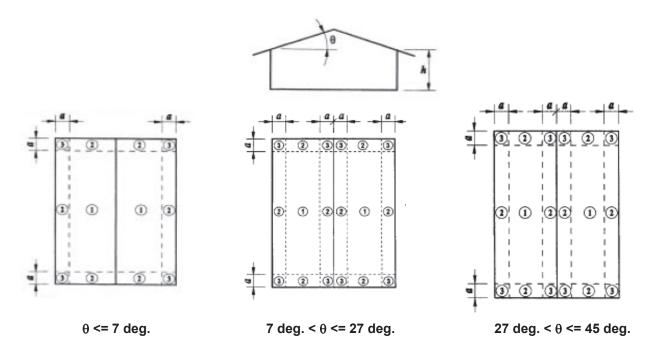
	Wind Lo	Wind Load Tabulation for Roof Components & Cladding					
Component	Z	Kh	qh	p =	= Net Design	Pressures (p	osf)
	(ft.)		(psf)	Zone 1,2,3 (+)	Zone 1 (-)	Zone 2 (-)	Zone 3 (-)
Decking	0	0.93	28.07	25.14	-27.82	-33.43	-33.43
	15.00	0.93	28.07	25.14	-27.82	-33.43	-33.43
	20.00	0.93	28.07	25.14	-27.82	-33.43	-33.43
	25.00	0.93	28.07	25.14	-27.82	-33.43	-33.43
For $z = he$:	20.00	0.93	28.07	25.14	-27.82	-33.43	-33.43
For $z = h$:	22.74	0.93	28.07	25.14	-27.82	-33.43	-33.43

Notes: 1. (+) and (-) signs signify wind pressures acting toward & away from respective surfaces.

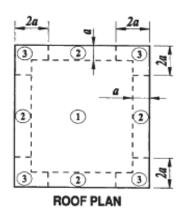
- 2. Width of Zone 2 (edge), 'a' =
- 3.00 ft. 3. Width of Zone 3 (corner), 'a' = 3.00 ft.
- 4. For monoslope roofs with $\theta \le 3$ degrees, use Fig. 30.4-2A for 'GCp' values with 'qh'.
- 5. For buildings with h > 60' and θ > 10 degrees, use Fig. 30.6-1 for 'GCpi' values with 'qh'.
- 6. For all buildings with overhangs, use Fig. 30.4-2B for 'GCp' values per Sect. 30.10.
- 7. If a parapet >= 3' in height is provided around perimeter of roof with $\theta \le 10$ degrees, Zone 3 shall be treated as Zone 2.
- 8. Per Code Section 30.2.2, the minimum wind load for C&C shall not be less than 16 psf.
- 9. References : a. ASCE 7-02, "Minimum Design Loads for Buildings and Other Structures".
 - b. "Guide to the Use of the Wind Load Provisions of ASCE 7-02" by: Kishor C. Mehta and James M. Delahay (2004).

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Roof Components and Cladding:



Roof Zones for Buildings with h <= 60 ft. (for Gable Roofs <= 45° and Monoslope Roofs <= 3°)



Roof Zones for Buildings with h > 60 ft. (for Gable Roofs \leq 10° and Monoslope Roofs \leq 3°)

Frame Design				General Info	
Cust. Name:	Bowers Engineering Se	rvices	Subject:	Roof Mount	
Job Number:	5416		Originator:		Checker:
Date:	1/10/22				
Address	14 Gloucester Ct	Rev:	-		
City, State:	Cameron, NC 28326				

Roof Rafter

			Roof	Loads		
Rafter Size=	2x4	SYP #1	Γ	ead Load=	8.00	psf
				Live Load=	20	psf
Trib. Area=	2	ft	Sı	now Load=	10	psf
Rafter length=	8.5	ft				
	(1.00	10		mbination	20.5	0
w=	61.00	plf	D+0.	75L+0.75S	30.5	psf
M=	550.91	lb-ft		EI=	8.6E+06	ib-in
Dead Load	l Roof Materials			$S_X =$	3.0625	10-111
Sheathing=	2	psf		$C_{M}=$	1.0	
Aspahlt Shingles=	3	psf		Cr=	1.2	
Insulation=	0.50	psf		$C_D =$	1.15	
Solar Panels=	2.50	psf		$C_F =$	1.3	
Assume Ligh	t-frame wood roof			$C_L =$	1.0	
	M 12			Fb=	1500	psi
f	$b = \frac{M * 12}{Sx}$					
			fb=	2158.65	psi	
F'b = Fb * Cd	*Cr*Cf*Cm*Cl		F'b=	2578.88	psi	OK
$5wl^{4}$	$\Delta L =$		0.55 in			
384 <i>EI</i>	$\Delta S=$		0.27 in			
50121	$\Delta D + L =$		0.77 in			
					<u>l/120</u>	
	$\Delta_{ m allow \ in} =$	0.77	<		0.85	OK
					<u>l/180</u>	
	$\Delta_{ m allow \ in} =$	0.55	<		0.57	OK

a

2 o/c

OK

2x4

^{*}Assume rafters are fully braced*

BES		Date:	1/10/2022	Connections
121 South Main ST				
Auburn, IN				
Cust. Name:	Bowers Engineering Services	Subject: R	oof Mount	
Job Number:	5416	Originator	0	Checker:
	STRUCTURAL SU	<u> IVIIVIAK Y</u>		
CODE SPEC				
	WIND			
IBC 2015	Sı	peed: 118 M	PH	

ASCE 7-10 Exp.: C

Risk Cat:

Wind Load - uplift

		Max lb
Zone 1	-27.49 psf	-184.71 lb
Zone 2	-33.03 psf	-221.98 lb
Zone 3	-33.03 psf	-221.98 lb
Max trib	11.20 ft2	

Max loading at connection

Negitive -221.98 lb/fastener

Connection (Pull Out)

Lag screw 5/16 in

Cd 1.60 Table 2.3.2

embedment 2.5 in

Nominal CapacityPrying 205.00 lbs G=0.42

Max capacity (lbs) 533.00 > 221.98 OK

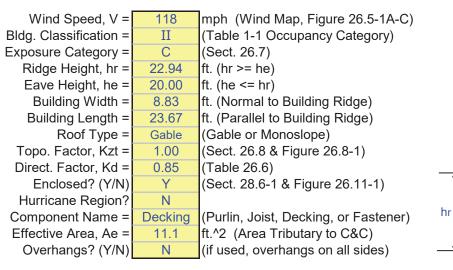
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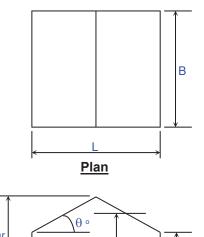
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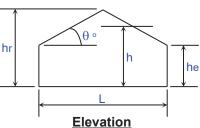
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BES			/	WIND LOAD	ING
121 South Main ST				Per ASCE 7-	-10
Auburn, IN					
Cust Name:	Bowers Engineering Services	Subject:	Roof Mount		
Job Number:	5416	Originator:	0	Checker:	

Input Data:







Resulting Parameters and Coefficients:

```
Roof Angle, \theta = 33.69 deg.
Mean Roof Ht., h = 21.47 ft. (h = (hr+he)/2, for roof angle >10 deg.)
```

Roof External Pressure Coefficients, GCp:

```
GCp Zone 1-3 Pos. = 0.90 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
GCp Zone 1 Neg. = -0.99 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
GCp Zone 2 Neg. = -1.19 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
GCp Zone 3 Neg. = -1.19 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
Positive & Negative Internal Pressure Coefficients, GCpi (Figure 26.11-1):
```

+GCpi Coef. = 0.00 (positive internal pressure)

-GCpi Coef. = 0.00 (negative internal pressure) If $z \le 15$ then: $Kz = 2.01*(15/zg)^{\alpha}(2/\alpha)$, If z > 15 then: $Kz = 2.01*(z/zg)^{\alpha}(2/\alpha)$ (Table 30.3-1)

 $\alpha = \begin{vmatrix} 9.50 \\ zg = \end{vmatrix}$ (Table 26.9-1) Kh = 0.92 (Kh = Kz evaluated at z = h)

Velocity Pressure: $qz = 0.00256*Kz*Kzt*Kd*V^2$ (Sect. 30.3.2, Eq. 30.3-1) qh = 27.74 psf $qh = 0.00256*Kh*Kzt*Kd*V^2$ (qz evaluated at z = h)

Design Net External Wind Pressures (Sect. 30.4 & 30.6):

For h <= 60 ft.: p = qh*((GCp) - (+/-GCpi)) (psf) For h > 60 ft.: p = q*(GCp) - qi*(+/-GCpi) (psf)

where: q = qh for roof

gi = gh for roof (conservatively assumed per Sect. 30.6)

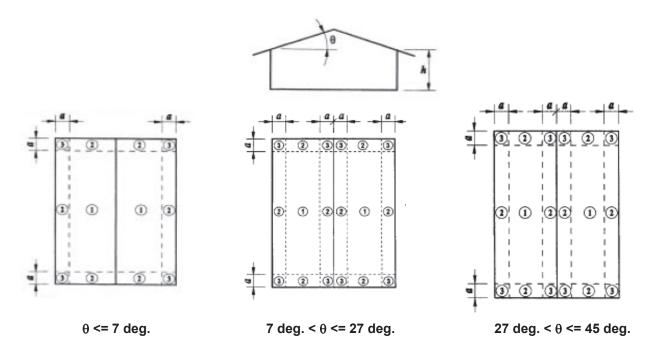
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Component	Z	Kh	qh	p =	= Net Design	Pressures (p	osf)
	(ft.)		(psf)	Zone 1,2,3 (+)	Zone 1 (-)	Zone 2 (-)	Zone 3 (-)
Decking	0	0.92	27.74	24.84	-27.49	-33.03	-33.03
	15.00	0.92	27.74	24.84	-27.49	-33.03	-33.03
	20.00	0.92	27.74	24.84	-27.49	-33.03	-33.03
For $z = hr$:	22.94	0.92	27.74	24.84	-27.49	-33.03	-33.03
For $z = he$:	20.00	0.92	27.74	24.84	-27.49	-33.03	-33.03
For $z = h$:	21.47	0.92	27.74	24.84	-27.49	-33.03	-33.03

Notes: 1. (+) and (-) signs signify wind pressures acting toward & away from respective surfaces.

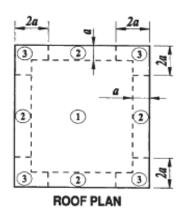
- 2. Width of Zone 2 (edge), 'a' =
- 3. Width of Zone 3 (corner), 'a' =
- 3.00 ft. 3.00 ft.
- 4. For monoslope roofs with $\theta \le 3$ degrees, use Fig. 30.4-2A for 'GCp' values with 'qh'.
- 5. For buildings with h > 60' and θ > 10 degrees, use Fig. 30.6-1 for 'GCpi' values with 'qh'.
- 6. For all buildings with overhangs, use Fig. 30.4-2B for 'GCp' values per Sect. 30.10.
- 7. If a parapet >= 3' in height is provided around perimeter of roof with $\theta \le 10$ degrees, Zone 3 shall be treated as Zone 2.
- 8. Per Code Section 30.2.2, the minimum wind load for C&C shall not be less than 16 psf.
- 9. References : a. ASCE 7-02, "Minimum Design Loads for Buildings and Other Structures".
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Roof Components and Cladding:



Roof Zones for Buildings with h <= 60 ft. (for Gable Roofs <= 45° and Monoslope Roofs <= 3°)



Roof Zones for Buildings with h > 60 ft. (for Gable Roofs \leq 10° and Monoslope Roofs \leq 3°)

Frame Design				General Info	
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Job Number:	5416		Originator:		Checker:
Date:	1/10/22				
Address	14 Gloucester Ct	Rev:	-		
City, State:	Cameron, NC 28326				

Roof Rafter

			<u>Rooj</u>	f Loads		
Rafter Size=	2x4	SYP #1	I	Dead Load=	8.00	psf
				Live Load=	20	psf
Trib. Area=	2	ft	S	Snow Load=	10	psf
Rafter length=	8.5	ft				
				ombination		
w=	61.00	plf	D+0	.75L+0.75S	30.5	psf
M=	550.91	lb-ft		D.	0.65.06	., .
D 11 1	D CM (1 1			EI=	8.6E+06	ib-in
	Roof Materials			$S_X =$	3.0625	
Sheathing=	2	psf		$C_{M}=$	1.0	
Aspahlt Shingles=	3	psf		Cr=	1.2	
Insulation=	0.50	psf		$C_D =$	1.15	
Solar Panels=	2.50	psf		$C_F =$	1.3	
Assume Light	t-frame wood roof			$C_L =$	1.0	
	M . 12			Fb=	1500	psi
fi	$b = \frac{M * 12}{Sx}$					_
, .	Sx		fb=	2158.65	psi	
F'b = Fb * Cd	*Cr*Cf*Cm*Cl]	F'b=	2578.88	psi	OK
4						
$5wl^4$	$\Delta L =$		0.55 in			
384 <i>EI</i>	$\Delta S =$		0.27 in			
	$\Delta D + L =$. (0.77 in		1/120	
		0.77			<u>1/120</u>	OIZ
	$\Delta_{ m allow\ in} =$	0.77	<		0.85	OK
		0			<u>l/180</u>	0.77
	$\Delta_{ m allow\ in}=$	0.55	<		0.57	OK

a

2 o/c

OK

2x4

^{*}Assume rafters are fully braced*

BES		Date:	1/10/2022	Connections
121 South Main ST				
Auburn, IN				
Cust. Name:	Bowers Engineering Services	Subject: Ro	of Mount	
Job Number:	5416	Originator	0	Checker:
	<u>STRUCTURAL SU</u>			
CODE SPEC				
CODE SPEC	WIND			

Exp.:

 \mathbf{C}

Wind Load - uplift

ASCE 7-10

Risk Cat:

Max lb

Zone 1 -25.49 psf -171.27 lb

Zone 2 -30.63 psf -205.84 lb

Zone 3 -30.63 psf -205.84 lb

Max trib 11.20 ft2

Max loading at connection

Negitive -205.84 lb/fastener

Connection (Pull Out)

Lag screw 5/16 in

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embedment 2.5 in

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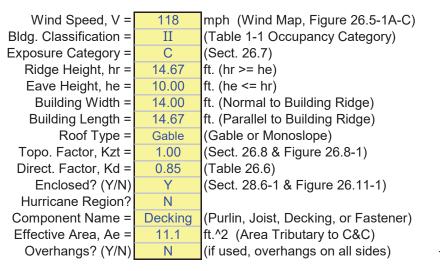
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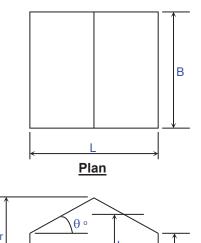
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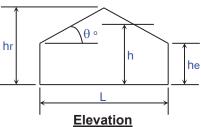
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BES			\	WIND LOADING	
121 South Main ST		Per ASCE 7-10			
Auburn, IN					
Cust Name:	Bowers Engineering Services	Subject:	Roof Mount		
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Resulting Parameters and Coefficients:

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Roof Angle, \theta = 33.69 deg.
Mean Roof Ht., h = 12.33 ft. (h = (hr+he)/2, for roof angle >10 deg.)
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Roof External Pressure Coefficients, GCp:

Kh =

```
GCp Zone 1-3 Pos. = 0.90 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C) GCp Zone 1 Neg. = -0.99 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C) GCp Zone 2 Neg. = -1.19 (Fig. 30.4-2A, 30.4-2B, and 30.4-2C) (Fig. 30.4-2A, 30.4-2B, and 30.4-2C) (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
```

Positive & Negative Internal Pressure Coefficients, GCpi (Figure 26.11-1):

```
+GCpi Coef. = 0.00 (positive internal pressure)

-GCpi Coef. = 0.00 (negative internal pressure)

If z \le 15 then: Kz = 2.01*(15/zg)^{2}(2/\alpha), If z > 15 then: Kz = 2.01*(z/zg)^{2}(2/\alpha) (Table 30.3-1)

\alpha = 9.50 (Table 26.9-1)

zg = 900 (Table 26.9-1)
```

Velocity Pressure: $qz = 0.00256*Kz*Kzt*Kd*V^2$ (Sect. 30.3.2, Eq. 30.3-1) qh = 25.72 psf $qh = 0.00256*Kh*Kzt*Kd*V^2$ (qz evaluated at z = h)

(Kh = Kz evaluated at z = h)

```
Design Net External Wind Pressures (Sect. 30.4 & 30.6):
For h \le 60 ft.: p = qh^*((GCp) - (+/-GCpi)) (psf)
For h \ge 60 ft.: p = q^*(GCp) - qi^*(+/-GCpi) (psf)
```

0.85

where: q = qh for roof

qi = qh for roof (conservatively assumed per Sect. 30.6)

Wind Load Tabulation for Roof Components & Cladding								
Component	Z	Kh	qh	p = Net Design Pressures (psf)				
	(ft.)		(psf)	Zone 1,2,3 (+)	Zone 1 (-)	Zone 2 (-)	Zone 3 (-)	
Decking	0	0.85	25.72	23.03	-25.49	-30.63	-30.63	
For $z = hr$:	14.67	0.85	25.72	23.03	-25.49	-30.63	-30.63	
For $z = he$:	10.00	0.85	25.72	23.03	-25.49	-30.63	-30.63	
For $z = h$:	12.33	0.85	25.72	23.03	-25.49	-30.63	-30.63	

ft.

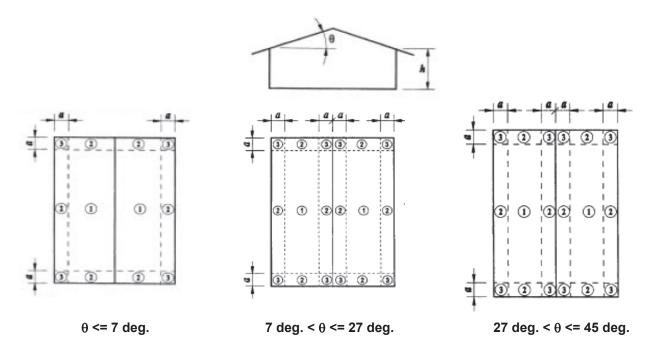
ft.

Notes: 1. (+) and (-) signs signify wind pressures acting toward & away from respective surfaces.

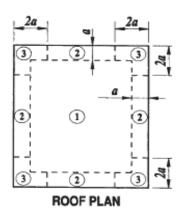
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- 3.00 3. Width of Zone 3 (corner), 'a' = 3.00
- 4. For monoslope roofs with $\theta \le 3$ degrees, use Fig. 30.4-2A for 'GCp' values with 'qh'.
- 5. For buildings with h > 60' and θ > 10 degrees, use Fig. 30.6-1 for 'GCpi' values with 'qh'.
- 6. For all buildings with overhangs, use Fig. 30.4-2B for 'GCp' values per Sect. 30.10.
- 7. If a parapet >= 3' in height is provided around perimeter of roof with $\theta \le 10$ degrees, Zone 3 shall be treated as Zone 2.
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Roof Components and Cladding:



Roof Zones for Buildings with h <= 60 ft. (for Gable Roofs <= 45° and Monoslope Roofs <= 3°)



Roof Zones for Buildings with h > 60 ft. (for Gable Roofs \leq 10° and Monoslope Roofs \leq 3°)

Frame Design General Info					
Cust. Name:	Bowers Engineering Se	Subject:	Roof Mount		
Job Number:	5416		Originator:		Checker:
Date:	1/10/22				
Address	14 Gloucester Ct	Rev:	-		
City, State:	Cameron, NC 28326				

Roof Rafter

		Roof Loads				
Rafter Size=	2x4	SYP #1		Dead Load=	8.00	psf
				Live Load=	20	psf
Trib. Area=	2	ft		Snow Load=	10	psf
Rafter length=	8.5	ft				
				d Combination		
w=	61.00	plf	I	D+0.75L+0.75S	30.5	psf
M=	550.91	lb-ft			0.67.06	
D 11	ID 016 11			EI=	8.6E+06	ib-in
	l Roof Materials			$S_X =$	3.0625	
Sheathing=	2	psf		$C_{M}=$	1.0	
Aspahlt Shingles=	3	psf		Cr=	1.2	
Insulation=	0.50	psf		$C_D =$	1.15	
Solar Panels=	2.50	psf		$C_F =$	1.3	
Assume Ligh	t-frame wood roof			$C_L =$	1.0	
	M . 12			Fb=	1500	psi
f	$b = \frac{M * 12}{Sx}$					
			fb=	2158.65	psi	
F'b = Fb * Cd * Cr * Cf * Cm * Cl			F'b=	2578.88	psi	OK
r14	$\Delta L =$		0.55 iı	•		
$\frac{5wl^4}{}$	$\Delta L - \Delta S =$		0.33 ii 0.27 ii			
384 <i>EI</i>	$\Delta D+L=$		0.27 ii 0.77 ii			
	ΔD · L		0.77 11	1	<u>l/120</u>	
	$\Delta_{ m allow \ in} =$	0.77	<		0.85	OK
	∸allow in	0.77			<u>l/180</u>	
	$\Delta_{ m allowin} =$	0.55	<		0.57	OK
	∸allow in	0.55	Ì		0.57	OIL

a

2 o/c

OK

2x4

^{*}Assume rafters are fully braced*