RIGHT ANGLE ENGINEERING

September 23, 2021

Power Home Solar and Roofing
919 North Main Street
Mooresville, NC 28115

RE: Structural Roof Evaluation for the *Russell Residence: 206 Clearview Court, Sanford, North Carolina*

As per your request, we have evaluated the roof structure under the proposed solar panel array. The information used to evaluate this structure was gathered by Power Home Solar and Roofing on behalf of Right Angle Engineering. The roof structure consists of 2x6 rafters spaced at 16" on center. The roof material consists of asphalt shingles. The design criteria used to analyze this structure are listed above and included with this letter. The adopted building codes in this jurisdiction are: *the 2018 North Carolina Building Code, the 2018 North Carolina Existing Building Code,* and *ASCE 7-16*.

North Carolina Existing Building Code (NCEBC) 2018 section 807.4 indicates that alterations to an existing building that results in less than a 10% increase in the total stress may be performed without a structural evaluation of the existing building. As demonstrated in the attached calculations, the additional weight of the solar panels will be less than 10% increase in the gravity loading and the stress on the existing roof framing.

Based on our assessment we have determined that the existing roof framing will safely and adequately support the additional loads imposed by the solar panels without reinforcement. In order for the loads to be evenly distributed, the roof attachments should be staggered and spread evenly throughout the panel array. Attachment points should be spaced at a maximum of 48" on center. The racking system should be installed per the manufacture's specifications. There should be a minimum of 35 L-foot attachment points to the roof. Each attachment should have a 5/16" or 18/8 SS lag screw with 2.5" minimum penetration centered on each truss top chord or rafter. Waterproofing around the roof penetrations is the responsibility of others. Right Angle Engineering assumes no responsibility for improper installation of the solar panels.

Regards,

9/23/21

Robert D Smythe, P.E.
Right Angle Engineering

Design Criteria:

Design Wind Speed (3 second gust)	115	mph
Exposure Category	C	
Risk Category	2	
Mean Roof Height	30	ft
Roof Type	Gable Roof	
Building Type	enclosed	

Roof Dead Load- ASCE Table C3-1

Asphalt Shingles	2	psf
5/8" Plywood Sheathing	2	psf
Roof Framing	4	psf
Insulation	0	psf
Gypsum sheathing	0	psf
Solar Panel Array	3	psf
Dead Load Without Panels	8	psf
Dead Load With Solar panels	11	psf

Roof Live Load

Existing Roof Live Load	20	psf	ASCE 7-16 Table 4.3-1
Roof Live Load with Solar Panels	0	psf	2018 NCBC 1607.12.5

Roof Snow Load-ASCE 7-16

Ground Snow Load (pg)	15	psf	Section 7.2
Exposure Factor (Ce)	0.9		Table 7.3-1
Thermal Factor (Ct)	1.1		Table 7.3-2
Importance Factor (Is)	1		Table 1.5-2
Flat Roof Snow Load (Pf)	10		Equation 7.3-1
Slippery surface Slope Factor (Cs)	0.47		Figure 7-2
Nonslippery Surface Slope Factor (Cs)	0.86		Figure 7-2
Roof Snow Load	9	psf	Equation 7.4-1
Reduced Roof Snow Load (Slippery Surface)	5	psf	Equation 7.4-1

Load Combinations - ASCE 7-16 Section 2.4.1

	Without Solar Panels	With Solar panels
D + Lr	28 psf	11 psf
D + S	17 psf	15.9 psf

Solar Array 1- Roof 1

Roof Slope	45	degrees
Number of panels	14	
Panel Area	245	ft^2

Wind Calculations- ASCE 7-16

GC_p Zone 1	-1		Figure 30.3-(2A-5B)
GC_p Zone 2	-1.8		Figure 30.3-(2A-5B)
GC_p Zone 3	-2.8		Figure 30.3-(2A-5B)
Gcpi	0.18		Table 26.13-1
Velocity Pressure (q_h)	28.2	psf	
$q_h = .00256 K_h K_{ht} K_d V^2$			Equation 26.10-1
K_h	0.98		Table 26.10-1
K_{ht}	1		Equation 26.8-1
K_d	0.85		Table 26.6-1
Designed wind pressure (P)		psf	Equation 30.8-1
$P = q_h(GC_h) - (GC_{hi}))$			
Zone 1 Pressure (P)	-33.3	psf	
Zone 2 Pressure (P)	-55.8	psf	
Zone 3 Pressure (P)	-84	psf	

Roof Connection

Shear Capacity	190	lbs	NDS 2015 Table 12K
Shear tributary area	34.2	ft^2	
Pullout Capacity	266	lbs/in	
Lag screw embedment	2.5	in	
Total pullout capacity	665	lbs	NDS 2015 Table 12.2A
Pullout max tributary area	11.9	ft^2	
Factor of Safety	1.71		
Minimum number of connections	**23**		

Beam Stress NCEBC 2018 Section 806.2

Beam Span	20	ft
Spacing	1.33	ft
Roof Framing type	2x6 rafters	
Panel Orientation	landscape	
Number of Panels per rafter	3	
Panel distance from eave	1	

	Without Solar Panels	With Solar Panels	Percent Increase	
Bending Moment	1862 ft-lbs	1489.7 ft-lbs	80%	Less than 105%
Vertical Reaction (V1)	372.4 lbs	325.2 lbs	87.3%	Less than 105%
Vertical Reaction (V2)	372.4 lbs	256.07 lbs	68.8%	Less than 105%

Solar Array 2- Roof 2

Roof Slope	42	degrees
Number of panels	7	
Panel Area	122.5	ft^2

Wind Calculations- ASCE 7-16

GC_p Zone 1	-1		Figure 30.3-(2A-5B)
GC_p Zone 2	-1.2		Figure 30.3-(2A-5B)
GC_p Zone 3	-1.2		Figure 30.3-(2A-5B)
Gcpi	0.18		Table 26.13-1
Velocity Pressure (q_h)	28.2	psf	
$q_h = .00256 K_h K_{ht} K_d V^2$			Equation 26.10-1
K_h	0.98		Table 26.10-1
K_{ht}	1		Equation 26.8-1
K_d	0.85		Table 26.6-1
Designed wind pressure (P)		psf	Equation 30.8-1
$P = q_h(GC_h) - (GC_{hi})$			
Zone 1 Pressure (P)	-33.3	psf	
Zone 2 Pressure (P)	-38.9	psf	
Zone 3 Pressure (P)	-38.9	psf	

Lag Screw Connection

Shear Capacity	190	lbs	NDS 2015 Table 12K
Shear tributary area	36.2	ft^2	
Pullout Capacity	266	lbs/in	
Lag screw embedment	2.5	in	
Total pullout capacity	665	lbs	NDS 2015 Table 12.2A
Pullout max tributary area	17.1	ft^2	
Factor of Safety	2.21		
Minimum number of connections	**11**		

Beam Stress NCEBC 2018 Section 806.2

Beam Span	24	ft
Spacing	1.33	ft
Roof Framing type	2x6 rafters	
Panel Orientation	landscape	
Number of Panels per rafter	4	
Panel distance from eave	10	

	Without Solar Panels	With Solar Panels	Percent Increase	
Bending Moment	2681.3 ft-lbs	2432.6 ft-lbs	90.7%	Less than 105%
Vertical Reaction (V1)	446.9 lbs	338.1 lbs	75.7%	Less than 105%
Vertical Reaction (V2)	446.9 lbs	390.5 lbs	87.4%	Less than 105%