

September 16, 2021

BES Project Number: 3119 Timothy Lemons

Power Home Solar, LLC 919 N Main St. Mooresville, NC 28115

> Project Location: Timothy Lemons: 38 Lone Pine Trail, Sanford, NC 27332 Solar Array Installation

To Whom It May Concern:

Per your request, BES has reviewed the existing structure at the above referenced location. The purpose of this review was to determine the adequacy of the existing structure to support the proposed installation of solar panels on the roof as shown on the attached panel layout plan.

Based upon our review, we certify that existing roof structure will adequately support with the following: Racking and attachment mounting connection: (1) 5/16" lag screw w/ min. 2.5" embedment into framing at max 48" o/c along rails (2) rails per row of panels, evenly spaced; panel length perpendicular to the rails not to exceed 67 in. Solar module mounting hardware design is by the manufacturer.

Limitations: Installation of the solar panels must be performed in accordance with manufacturer recommendations. All work performed must be in accordance with accepted industry-wide methods and applicable safety standards. The contractor must notify BES should any damage, deterioration or discrepancies between the as-built condition of the structure and the condition described in this letter be found. Connections to existing roof framing must be staggered, except at array ends, so as to not overload any existing structural member. The design of the solar panel racking (mounts, rails, etc.) is the responsibility of the manufacturer. Waterproofing around the roof penetrations is the responsibility of others. BES assumes no responsibility for improper installation of the solar array. Existing structure meets or exceeds standard building practices with current building code with assumed single layer asphalt shingles.

Sincerely,



Jermey Bowers M.E., P.E. *Principal Engineer*

Bowers Engineering Services 121 S. Main ST Auburn, IN (260) 333-0900

Structural Analysis

Location

38 Lone Pine Trail Sanford, NC 27332

Roof Mount Solar

9/16/2021



Project: 3119 Timothy Lemons Rev: -

BES		Date:	9/16/2021	Connections
121 South Main ST				
Auburn, IN				
Cust. Name:	Bowers Engineering Services	Subject:	Roof Mount	
Job Number:	3119 Timothy Lemons	Originator	0	Checker:

STRUCTURAL SUMMARY

CODE SPEC

WIND

IBC 2015 Speed: 116 MPH

ASCE 7-10 Exp.: C

Risk Cat:

Wind Load - uplift

		Max lb
Zone 1	-26.71 psf	-179.49 lb
Zone 2	-32.10 psf	-215.71 lb
Zone 3	-32.10 psf	-215.71 lb
Max trib	11.20 ft2	

Max loading at connection

Negitive -215.71 lb/fastener

Connection (Pull Out)

Lag screw 5/16 in

Cd 1.60 Table 2.3.2

embedment 2.5 in

Nominal CapacityPrying 205.00 lbs G=0.42

Max capacity (lbs) 533.00 > 215.71 **OK**

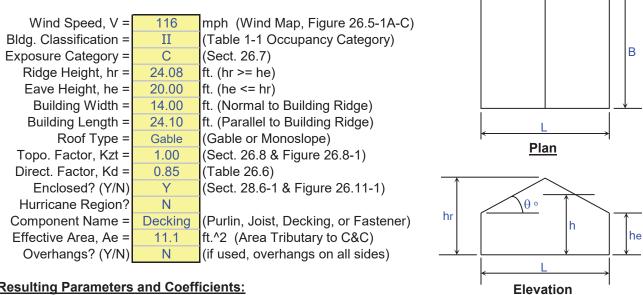
Note:

^{*} Lag screws to be diameter 5/16x2.5inches long.

^{*} All fasteners need to be placed at roof rafters.

BES			1	WIND LOADING
121 South Main ST				Per ASCE 7-10
Auburn, IN				
Cust Name:	Bowers Engineering Services	Subject:	Roof Mount	
Job Number:	3119 Timothy Lemons	Originator:	0	Checker:

Input Data:



Resulting Parameters and Coefficients:

```
Roof Angle, \theta =
                        30.26
Mean Roof Ht., h =
                        22.04
                                 ft. (h = (hr+he)/2, for roof angle >10 deg.)
```

Roof External Pressure Coefficients, GCp:

0.90

GCp Zone 1-3 Pos. =

```
-0.99
                                    (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
   GCp Zone 1 Neg. =
   GCp Zone 2 Neg. =
                           -1.19
                                    (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
   GCp Zone 3 Neg. =
                           -1.19
                                    (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
Positive & Negative Internal Pressure Coefficients, GCpi (Figure 26.11-1):
        +GCpi Coef. =
                           0.00
                                    (positive internal pressure)
         -GCpi Coef. =
                           0.00
                                    (negative internal pressure)
If z \le 15 then: Kz = 2.01*(15/zg)^{2}(2/\alpha), If z > 15 then: Kz = 2.01*(z/zg)^{2}(2/\alpha) (Table 30.3-1)
                                    (Table 26.9-1)
                    \alpha =
                           9.50
                            900
                                    (Table 26.9-1)
                   zg =
```

(Fig. 30.4-2A, 30.4-2B, and 30.4-2C)

```
Velocity Pressure: qz = 0.00256*Kz*Kzt*Kd*V^2 (Sect. 30.3.2, Eq. 30.3-1)
                                           qh = 0.00256*Kh*Kzt*Kd*V^2 (qz evaluated at z = h)
                qh = 26.95 psf
```

(Kh = Kz evaluated at z = h)

```
Design Net External Wind Pressures (Sect. 30.4 & 30.6):
For h <= 60 ft.: p = qh^*((GCp) - (+/-GCpi)) (psf)
```

0.92

For
$$h > 60$$
 ft.: $p = q^*(GCp) - qi^*(+/-GCpi)$ (psf)

Kh =

where: q = qh for roof

qi = qh for roof (conservatively assumed per Sect. 30.6)

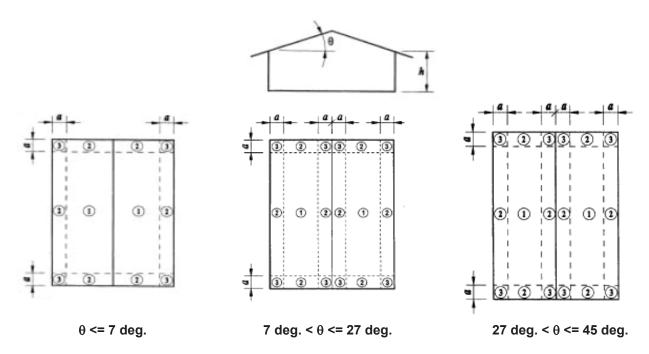
Wind Load Tabulation for Roof Components & Cladding							
Component	Z	Kh	qh	p =	= Net Design	Pressures (p	osf)
	(ft.)		(psf)	Zone 1,2,3 (+)	Zone 1 (-)	Zone 2 (-)	Zone 3 (-)
Decking	0	0.92	26.95	24.14	-26.71	-32.10	-32.10
	15.00	0.92	26.95	24.14	-26.71	-32.10	-32.10
	20.00	0.92	26.95	24.14	-26.71	-32.10	-32.10
For $z = hr$:	24.08	0.92	26.95	24.14	-26.71	-32.10	-32.10
For $z = he$:	20.00	0.92	26.95	24.14	-26.71	-32.10	-32.10
For $z = h$:	22.04	0.92	26.95	24.14	-26.71	-32.10	-32.10

Notes: 1. (+) and (-) signs signify wind pressures acting toward & away from respective surfaces.

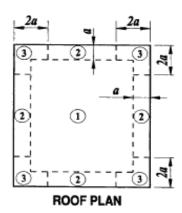
- 2. Width of Zone 2 (edge), 'a' =
- 3.00 lft. 3.00 3. Width of Zone 3 (corner), 'a' = ft.
- 4. For monoslope roofs with $\theta \le 3$ degrees, use Fig. 30.4-2A for 'GCp' values with 'qh'.
- 5. For buildings with h > 60' and θ > 10 degrees, use Fig. 30.6-1 for 'GCpi' values with 'qh'.
- 6. For all buildings with overhangs, use Fig. 30.4-2B for 'GCp' values per Sect. 30.10.
- 7. If a parapet >= 3' in height is provided around perimeter of roof with $\theta \le 10$ degrees, Zone 3 shall be treated as Zone 2.
- 8. Per Code Section 30.2.2, the minimum wind load for C&C shall not be less than 16 psf.
- 9. References : a. ASCE 7-02, "Minimum Design Loads for Buildings and Other Structures".
 - b. "Guide to the Use of the Wind Load Provisions of ASCE 7-02" by: Kishor C. Mehta and James M. Delahay (2004).

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Roof Components and Cladding:



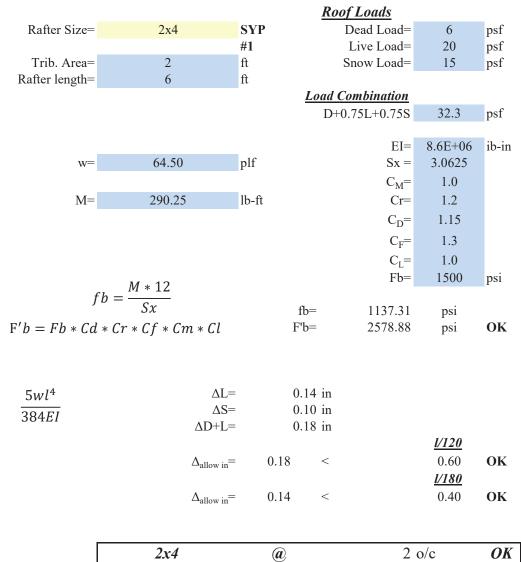
Roof Zones for Buildings with h \leq 60 ft. (for Gable Roofs \leq 45° and Monoslope Roofs \leq 3°)



Roof Zones for Buildings with h > 60 ft. (for Gable Roofs \leq 10° and Monoslope Roofs \leq 3°)

Frame Design				General Info)
Cust. Name:	Bowers Engineering Se	rvices	Subject:	Roof Mount	
Job Number:	3119 Timothy Lemons		Originator:		Checker:
Date:	44455				
Address	38 Lone Pine Trail	Rev:	-		
City, State:	Sanford, NC 27332				

Roof Rafter



^{*}Assume rafters are fully braced*

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Structural Analysis

Location

38 Lone Pine Trail Sanford, NC 27332

Roof Mount Solar

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Project: 3119 Timothy Lemons Rev: -

BES		Date:	9/16/2021	Connections
121 South Main ST				
Auburn, IN				
Cust. Name:	Bowers Engineering Services	Subject: R	oof Mount	
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STRUCTURAL SUMMARY

CODE SPEC

WIND

IBC 2015 Speed: 116 MPH

ASCE 7-10 Exp.: C

Risk Cat:

Wind Load - uplift

		Max 16
Zone 1	-26.86 psf	-180.52 lb
Zone 2	-32.28 psf	-216.95 lb
Zone 3	-32.28 psf	-216.95 lb
Max trib	11.20 ft2	

Max loading at connection

Negitive -216.95 lb/fastener

Connection (Pull Out)

Lag screw 5/16 in

Cd 1.60 Table 2.3.2

embedment 2.5 in

Nominal CapacityPrying 205.00 lbs G=0.42

Max capacity (lbs) 533.00 > 216.95

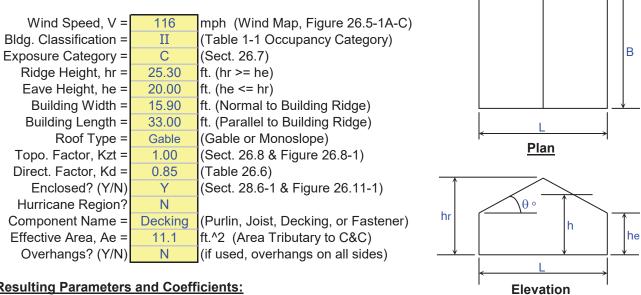
Note:

^{*} Lag screws to be diameter 5/16x2.5inches long.

^{*} All fasteners need to be placed at roof rafters.

BES			1	WIND LOADING
121 South Main ST				Per ASCE 7-10
Auburn, IN				
Cust Name:	Bowers Engineering Services	Subject:	Roof Mount	
Job Number:	3119 Timothy Lemons	Originator:	0	Checker:

Input Data:



Resulting Parameters and Coefficients:

```
Roof Angle, \theta =
                        33.69
Mean Roof Ht., h =
                        22.65
                                 ft. (h = (hr+he)/2, for roof angle >10 deg.)
```

Roof External Pressure Coefficients, GCp:

```
GCp Zone 1-3 Pos. =
                          0.90
                                  (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
                         -0.99
                                  (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
   GCp Zone 1 Neg. =
  GCp Zone 2 Neg. =
                         -1.19
                                  (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
   GCp Zone 3 Neg. =
                         -1.19
                                  (Fig. 30.4-2A, 30.4-2B, and 30.4-2C)
Positive & Negative Internal Pressure Coefficients, GCpi (Figure 26.11-1):
        +GCpi Coef. =
                          0.00
                                  (positive internal pressure)
```

```
-GCpi Coef. =
                             0.00
                                      (negative internal pressure)
If z \le 15 then: Kz = 2.01*(15/zg)^{2}(2/\alpha), If z > 15 then: Kz = 2.01*(z/zg)^{2}(2/\alpha) (Table 30.3-1)
                                      (Table 26.9-1)
                     \alpha =
                             9.50
                             900
                                      (Table 26.9-1)
                    zg =
                   Kh =
                             0.93
                                      (Kh = Kz evaluated at z = h)
```

```
Velocity Pressure: qz = 0.00256*Kz*Kzt*Kd*V^2 (Sect. 30.3.2, Eq. 30.3-1)
                                           qh = 0.00256*Kh*Kzt*Kd*V^2 (qz evaluated at z = h)
                qh = 27.11 psf
```

```
Design Net External Wind Pressures (Sect. 30.4 & 30.6):
For h <= 60 ft.: p = qh^*((GCp) - (+/-GCpi)) (psf)
```

For h > 60 ft.:
$$p = q^*(GCp) - qi^*(+/-GCpi)$$
 (psf)

where: q = qh for roof

qi = qh for roof (conservatively assumed per Sect. 30.6)

Wind Load Tabulation for Roof Components & Cladding							
Component	Z	Kh	qh	p =	= Net Design	Pressures (p	osf)
	(ft.)		(psf)	Zone 1,2,3 (+)	Zone 1 (-)	Zone 2 (-)	Zone 3 (-)
Decking	0	0.93	27.11	24.27	-26.86	-32.28	-32.28
	15.00	0.93	27.11	24.27	-26.86	-32.28	-32.28
	20.00	0.93	27.11	24.27	-26.86	-32.28	-32.28
	25.00	0.93	27.11	24.27	-26.86	-32.28	-32.28
For $z = he$:	20.00	0.93	27.11	24.27	-26.86	-32.28	-32.28
For $z = h$:	22.65	0.93	27.11	24.27	-26.86	-32.28	-32.28

Notes: 1. (+) and (-) signs signify wind pressures acting toward & away from respective surfaces.

- 2. Width of Zone 2 (edge), 'a' =
- 3. Width of Zone 3 (corner), 'a' = 3.00 ft.
- 4. For monoslope roofs with $\theta \le 3$ degrees, use Fig. 30.4-2A for 'GCp' values with 'qh'.
- 5. For buildings with h > 60' and θ > 10 degrees, use Fig. 30.6-1 for 'GCpi' values with 'qh'.

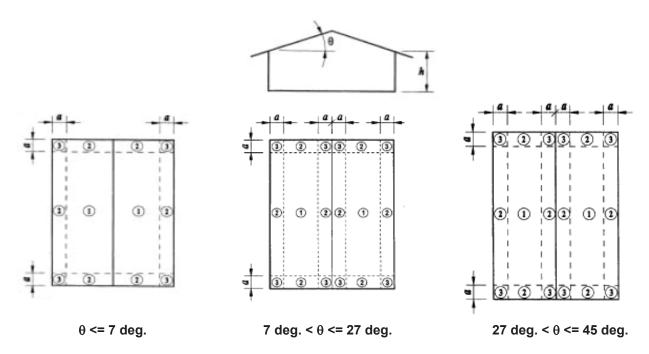
3.00

lft.

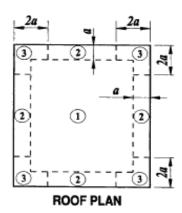
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- 7. If a parapet >= 3' in height is provided around perimeter of roof with $\theta \le 10$ degrees, Zone 3 shall be treated as Zone 2.
- 8. Per Code Section 30.2.2, the minimum wind load for C&C shall not be less than 16 psf.
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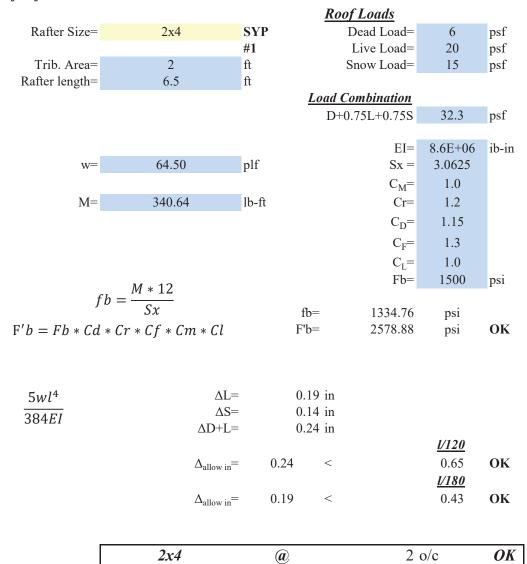
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Roof Rafter



^{*}Assume rafters are fully braced*