



BLUE RAVEN SOLAR, LLC
Firm License No. D-0396
1403 North Research Way
Building J
Orem, UT 84097

February 23, 2020

To: Blue Raven Solar
1403 N. Research Way, Bldg. J
Orem, UT. 84097

Subject: Certification Letter
Everette Residence
1118 Oak Grove Church Rd.
Angier, NC. 27501

To Whom It May Concern,

A jobsite observation of the condition of the existing framing system was performed by an audit team of Blue Raven Solar. All attached structural calculations are based on these observations and the design criteria listed below.

On the above referenced project, the roof structural framing has been reviewed for additional loading due to the installation of the solar PV addition to the roof. The structural review, including the plans and calculations only apply to the section of the roof that is directly supporting the solar PV system and its supporting elements. The observed roof framing is described below.

The roof structure of (MP1&2) consists of composition shingle on roof plywood that is supported by pre-manufactured trusses that are spaced at @ 24" o.c.. The top chords, sloped at 35 degrees, are 2x6 sections, the bottom chords are 2x4 sections and the web members are 2x4 sections. The truss members are connected by steel gusset plates. The max unsupported projected horizontal top chord span is approximately 9'-0".

The existing roof framing system of (MP1&2) are judged to be adequate to withstand the loading imposed by the installation of the solar panels. No reinforcement is necessary.

The spacing of the solar standoffs should be kept at 72" o.c. for landscape and 48" o.c. for portrait orientation, with a staggered pattern to ensure proper distribution of loads.

The scope of this report is strictly limited to an evaluation of the fastener attachment, underlying framing and supporting structure only. The attachment's to the existing structure are required to be in a staggered pattern to ensure proper distribution of loading. All panels, racking and hardware shall be installed per manufacturer specifications and within specified design limitations. All waterproofing shall be provided by the manufacturer.

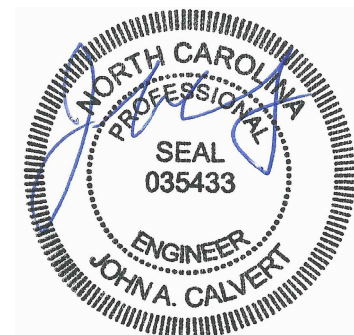
Design Criteria:

- Applicable Codes = 2018 North Carolina State Building Code (NCSBC), ASCE7-10, and NDS-12
- Roof Dead Load = 8 psf (MP1&2)
- Roof Live Load = 20 psf
- Wind Speed = 115 mph, Exposure C
- Ground Snow Load = 15 psf - Roof Snow Load = 10.5 psf
- Attachments: (1) 5/16" dia lag screw with 2.5" min embedment depth, at spacing shown above.

Please contact me with any further questions or concerns regarding this project.

Sincerely,

John Calvert, P.E.
Project Engineer





Gravity Loading

Roof Snow Load Calculations		
p_g = Ground Snow Load =	15 psf	
$p_f = 0.7 C_e C_t I p_g$		(ASCE7 - Eq 7-1)
C_e = Exposure Factor =	1	(ASCE7 - Table 7-2)
C_t = Thermal Factor =	1	(ASCE7 - Table 7-3)
I = Importance Factor =	1	
p_f = Flat Roof Snow Load =	10.5 psf	
$p_s = C_s p_f$		(ASCE7 - Eq 7-2)
C_s = Slope Factor =	1	
p_s = Sloped Roof Snow Load =	10.5 psf	

PV Dead Load = 3 psf (Per Blue Raven Solar)	
PV System Weight	
Weight of PV System (Per Blue Raven Solar)	3.0 psf
X Standoff Spacing =	4.00 ft
Y Standoff Spacing =	5.50 ft
Standoff Tributary Area =	22.00 sft
Point Loads of Standoffs	66 lb

Note: PV standoffs are staggered to ensure proper distribution of loading

Roof Live Load = 20 psf	
Note: Roof live load is removed in area's covered by PV array.	

Roof Dead Load (MP1&2)		
Composition Shingle	4.00	
Roof Plywood	2.00	
2x6 Top Chords @ 24"o.c.	1.15	
Vaulted Ceiling	0.00	(Ceiling Not Vaulted)
Miscellaneous	0.85	
Total Roof DL (MP1&2)	8.0 psf	
DL Adjusted to 35 Degree Slope	9.8 psf	

Wind Calculations

Per ASCE7-10 Components and Cladding

Input Variables	
Wind Speed	115 mph
Exposure Category	C
Roof Shape	Gable/Hip
Roof Slope	35 degrees
Mean Roof Height	20 ft
Effective Wind Area	19.3 ft

Design Wind Pressure Calculations	
Wind Pressure $P = qh * G * Cn$	
$qh = 0.00256 * Kz * Kzt * Kd * V^2$	(Eq. 30.3-1)
Kz (Exposure Coefficient) = 0.9	(Table 30.3-1)
Kzt (topographic factor) = 1	(Fig. 26.8-1)
Kd (Wind Directionality Factor) = 0.85	(Table 26.6-1)
V (Design Wind Speed) = 115 mph	(Fig. 26.5-1A)
Risk Category = II	(Table 1.5-1)
$qh = 25.90$	
$0.6 * qh = 15.54$	

Standoff Uplift Calculations-Portrait					
	Zone 1	Zone 2	Zone 3	Positive	
G_{Cp} =	-0.92	-1.12	-1.12	0.86	(Fig. 30.4-1)
Uplift Pressure =	-14.36 psf	-17.47 psf	-17.47 psf	22.3 psf	
X Standoff Spacing =	4.00	4.00	2.67		
Y Standoff Spacing =	5.50	2.75	2.75		
Tributary Area =	22.00	11.00	7.33		
Footing Uplift =	-316 lb	-192 lb	-128 lb		

Standoff Uplift Calculations-Landscape					
	Zone 1	Zone 2	Zone 3	Positive	
G_{Cp} =	-0.92	-1.12	-1.12	0.86	(Fig. 30.4-1)
Uplift Pressure =	-14.36 psf	-17.47 psf	-17.47 psf	10.0 psf	(Minimum)
X Standoff Spacing =	6.00	6.00	4.00		
Y Standoff Spacing =	3.50	1.75	1.75		
Tributary Area =	21.00	10.50	7.00		
Footing Uplift =	-302 lb	-183 lb	-122 lb		

Standoff Uplift Check	
Maximum Design Uplift =	-316 lb
Standoff Uplift Capacity =	450 lb
450 lb capacity > 316 lb demand Therefore, OK	

Fastener Capacity Check	
Fastener = 1 - 5/16" dia Lag	
Number of Fasteners =	1
Embedment Depth =	2.5
Pullout Capacity Per Inch =	250 lb
Fastener Capacity =	625 lb
w/ F.S. of 1.5 & DOL of 1.6=	667 lb
667.2 lb capacity > 316 lb demand Therefore, OK	

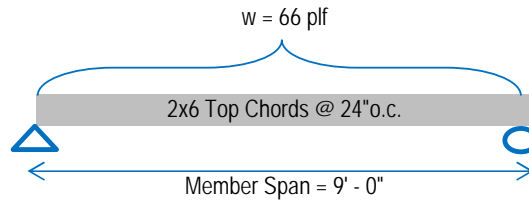


Framing Check

(MP1&2)

PASS

Dead Load 9.8 psf
 PV Load 3.0 psf
 Live Load 20.0 psf



Governing Load Combo = DL + LL
 Total Load 32.8 psf

Member Properties				
Member Size	S (in ³)	I (in ⁴)	Lumber Sp/Gr	Member Spacing
2x6	7.56	20.80	DF#2	@ 24" o.c.

Check Bending Stress								
Fb (psi) =	f _b	x	C _d	x	C _f	x	C _r	(NDS Table 4.3.1)
	900	x	1.25	x	1.3	x	1.15	
Allowed Bending Stress = 1681.8 psi								

Maximum Moment = $(wL^2) / 8$
 $= 663.515 \text{ ft}\#$
 $= 7962.19 \text{ in}\#$
 Actual Bending Stress = (Maximum Moment) / S
 $= 1052.9 \text{ psi}$

Allowed > Actual -- 62.7% Stressed -- Therefore, OK

Check Deflection	
Allowed Deflection (Total Load) =	$L/180$ (E = 1600000 psi Per NDS)
	= 0.6 in
Deflection Criteria Based on =	Continuous Span
Actual Deflection (Total Load) =	$(w \cdot L^4) / (185 \cdot E \cdot I)$
	= 0.121 in
	= L/893 > L/180 Therefore OK

Allowed Deflection (Live Load) =	$L/240$
	0.45 in
Actual Deflection (Live Load) =	$(w \cdot L^4) / (185 \cdot E \cdot I)$
	0.074 in
	L/1460 > L/240 Therefore OK

Check Shear		
Member Area = 8.3 in ²	F _v (psi) = 180 psi	(NDS Table 4A)
Allowed Shear = F _v * A = 1485 lb	Max Shear (V) = w * L / 2 =	295 lb

Allowed > Actual -- 19.9% Stressed -- Therefore, OK