

**SOIL/SITE EVALUATION  
 for ON-SITE WASTEWATER SYSTEM**

Owner: 08-500-19347

Applicant:

Address:

Date Evaluated: 2.20

Proposed Facility: SFO

Design Flow (.1949): 480

Property Size:

Location of Site: 1125

Property Recorded:

Water Supply:  Public  Individual  Well

Spring  Other

Evaluation Method:  Auger Boring  Pit

Cut

Type of Wastewater:  Sewage  Industrial Process

Mixed

| P<br>R<br>O<br>F<br>I<br>L<br>E<br># | .1940<br>Landscape<br>Position/<br>Slope% | Horizon<br>Depth<br>(IN.) | SOIL MORPHOLOGY<br>.1941       |                                    | OTHER<br>PROFILE FACTORS           |                              |                         |                         | Profile<br>Class<br>& LTAR |
|--------------------------------------|---|---------------------------|--------------------------------|------------------------------------|------------------------------------|------------------------------|-------------------------|-------------------------|----------------------------|
|                                      |   |                           | .1941<br>Structure/<br>Texture | .1941<br>Consistence<br>Mineralogy | .1942<br>Soil<br>Wetness/<br>Color | .1943<br>Soil<br>Depth (IN.) | .1956<br>Sapro<br>Class | .1944<br>Restr<br>Horiz |                            |
| 5<br>21                              |   | 0-48                      | GR SL                          | VFA SE                             |                                    |                              |                         |                         | .6                         |
|                                      |   | 0-48                      | GR SL                          | VFA SE                             |                                    |                              |                         |                         | .6                         |
|                                      |   | 0-48                      | GR SL                          | VFA SE                             |                                    |                              |                         |                         | .6                         |
|                                      |   | 0-48                      | GR SL                          | VFA SE                             |                                    |                              |                         |                         | .6                         |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |
|                                      |   |                           |                                |                                    |                                    |                              |                         |                         |                            |

| Description             | Initial System | Repair System |
|-------------------------|----------------|---------------|
| Available Space (.1945) | /              | /             |
| System Type(s)          | 251.           | 48            |
| Site LTAR               | .6             | .3            |

Other Factors (.1946): \_\_\_\_\_  
 Site Classification (.1948): P'  
 Evaluated By: JN  
 Others Present: P+ by J.M.M

1/210 + 251-

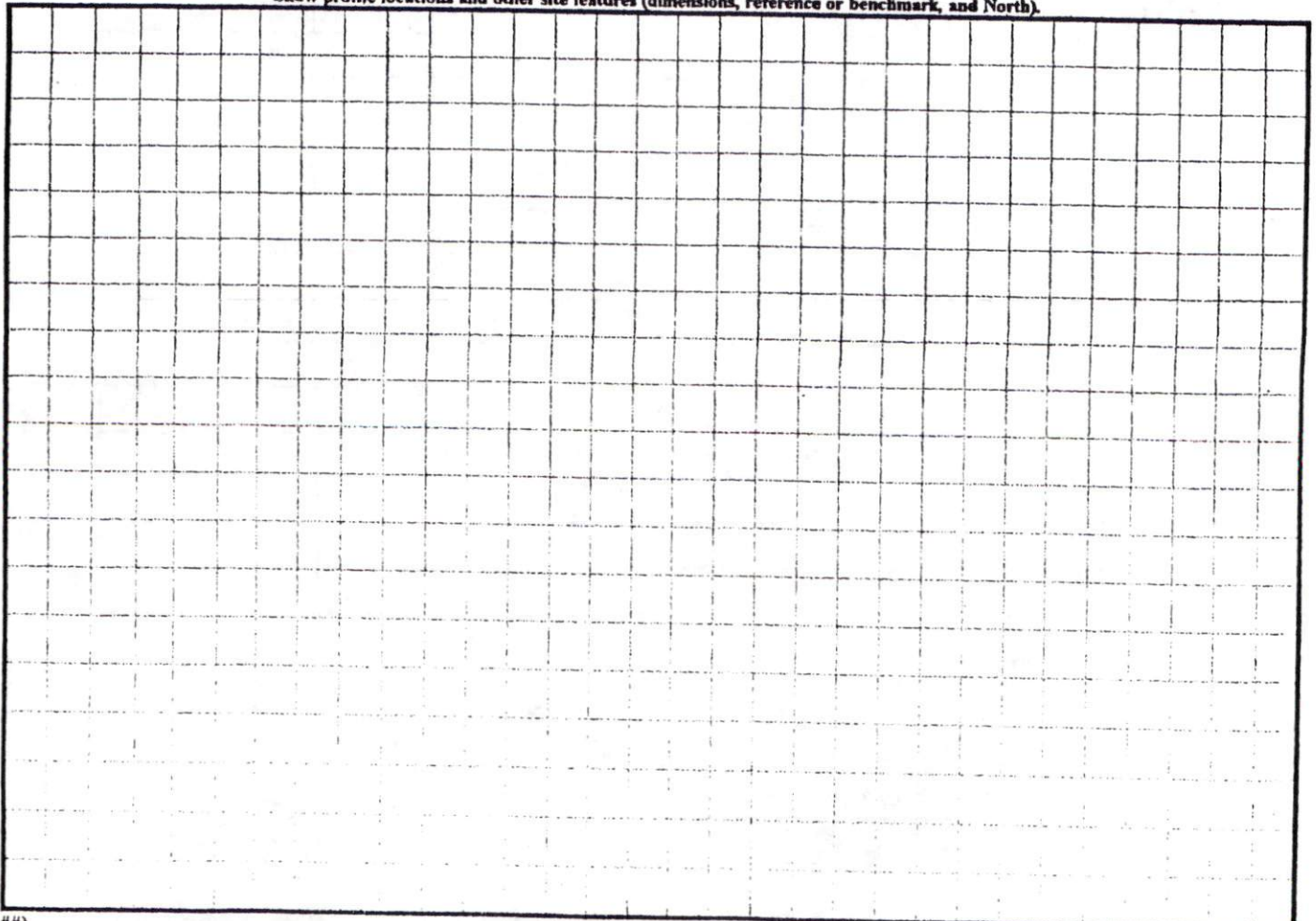
COMMENTS: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

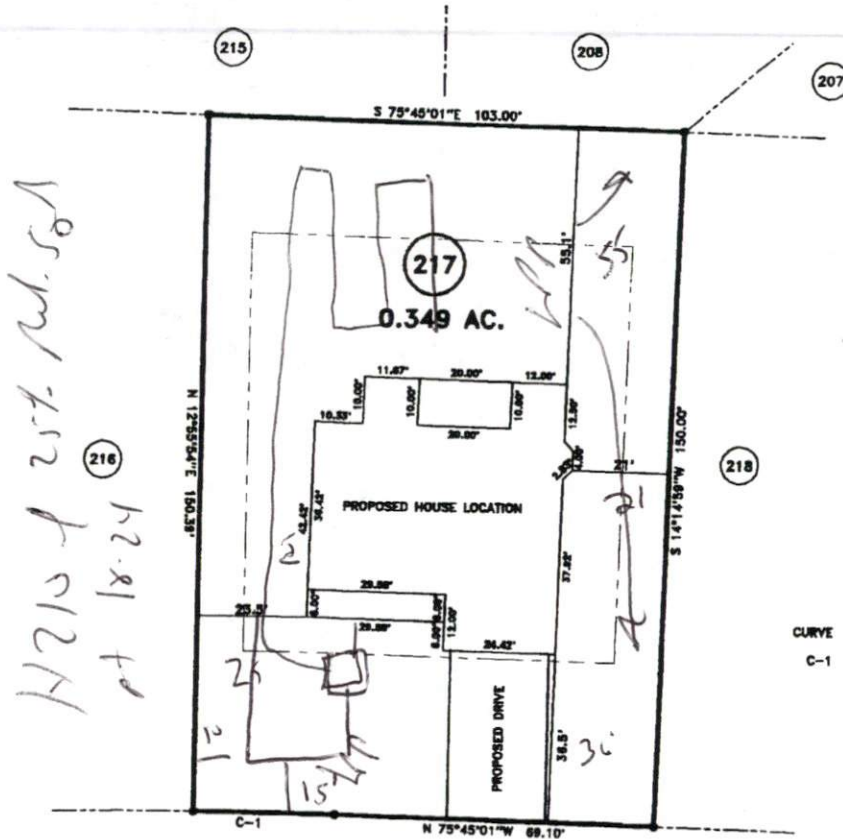
| <u>LANDSCAPE POSITIONS</u> | <u>GROUP</u> | <u>TEXTURES</u>  | <u>.1955 LTAR</u> | <u>CONSISTENCE MOIST</u> | <u>WET</u>         |
|----------------------------|--------------|--|-------------------|--------------------------|--------------------|
| R-RIDGE                    | I            | S-SAND   | 1.2 - 0.8         | VFR-VERY FRIABLE         | NS-NON-STICKY      |
| S-SHOULDER SLOPE           |              | LS-LOAMY SAND  |                   |                          |                    |
| L-LINEAR SLOPE             | II           | SL-SANDY LOAM  | 0.8 - 0.6         | FR-FRIABLE               | SS-SLIGHTLY STICKY |
| FS-FOOT SLOPE              |              | L-LOAM   |                   | FI-FIRM                  | S-STICKY           |
| N-NOSE SLOPE               | III          | SI-SILT-<br>SIL-SILT LOAM<br>CL-CLAY LOAM<br>SCL-SANDY CLAY LOAM<br>SICL-SILTY CLAY LOAM | 0.6 - 0.3         | VFI-VERY FIRM            | VS-VERY STICKY     |
| H-HEAD SLOPE               |              |  |                   | EFI-EXTREMELY FIRM       | NP-NON-PLASTIC     |
| CC-CONCLAVE SLOPE          |              |  |                   |                          | SP-SLIGHTLY STICKY |
| CV-CONVEX SLOPE            |              |  |                   |                          | P-PLASTIC          |
| T-TERRACE                  |              |  |                   |                          | VP-VERY PLASTIC    |
| FP-FLOOD PLAN              | IV           | SIC-SILTY CLAY   | 0.4 - 0.1         |                          |                    |
|                            |              | C-CLAY   |                   |                          |                    |
|                            |              | SC-SANDY CLAY  |                   |                          |                    |

STRUCTURE  
 SG-SINGLE GRAIN  
 M-MASSIVE  
 CR-CRUMB  
 GR-GRANULAR  
 SBK-SUBANGULAR BLOCKY  
 ABK-ANGULAR BLOCKY  
 PL-PLATY  
 PR-PRISMATIC

MINERALOGY  
 SLIGHTLY EXPANSIVE  
 EXPANSIVE

Show profile locations and other site features (dimensions, reference or benchmark, and North).





*H210 of 257. Rd. 581  
42.81 to  
18.24*

*103  
21  
242  
54  
25*

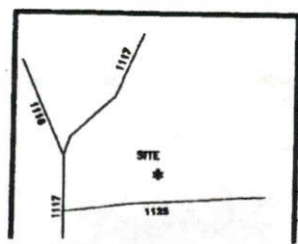
**SITE PLAN APPROVAL**  
 DISTRICT BASIC USE SFD  
 #BEDROOMS 4  
 Date 2/1/08  
 Zoning Administrator [Signature]

| CURVE | RADIUS   | LENGTH | CHORD  | CH. BEARING  |
|-------|----------|--------|--------|--------------|
| C-1   | 1323.42' | 30.44' | 30.44' | N 76°24'34"W |

MAP REFERENCE: MAP NO. 2007-948

"SONORA DRIVE" 50' R/W

**MINIMUM BUILDING SET BACKS**  
 FRONT YARD ——— 35'  
 REAR YARD ——— 20'  
 SIDE YARD ——— 10'  
 CORNER LOT SIDE YARD — 20'  
 MAXIMUM HEIGHT ——— 35'



|   |                        |   |               |
|---|------------------------|---|---------------|
| SURVEY FOR:<br><b>PROPOSED PLOT PLAN - LOT - 217</b><br><b>FOREST OAKS S/D, PHASE - 5</b> |                        | JOB NO. 08045<br><b>BENNETT SURVEYS, INC.</b><br>1662 CLARK RD., LILLINGTON, N.C. 27546<br>(910) 893-5252 |               |
| TOWNSHIP ANDERSON CREEK   | COUNTY HARNETT         | 20 0 40   | SURVEYED BY:  |
| STATE: NORTH CAROLINA   | DATE: JANUARY 30, 2007 |   | FIELD BOOK    |
|   |                        |   | DRAWN BY: RVB |